

Orbit control at IP

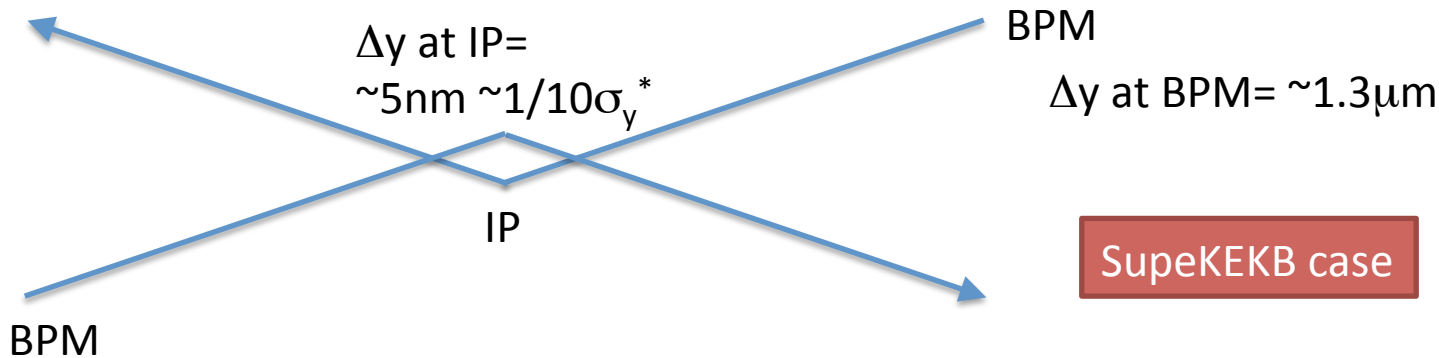
Y. Funakoshi
for the IP orbit control working group
The 17th KEKB Accelerator Review
Feb. 20 2012

Contents

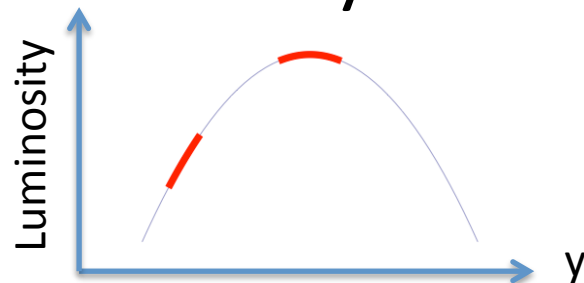
- Algorithm of orbit control
- QCS vibration issues
- Dithering method for luminosity FB

Orbit feedback at IP :Algorism

- Beam-beam deflection (SLC, KEKB vertical)

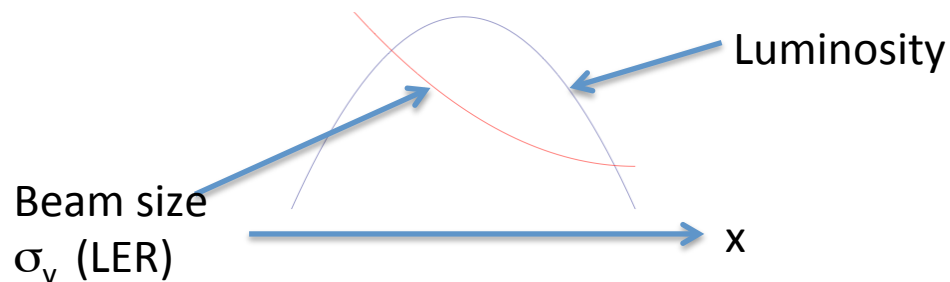


- Luminosity feedback (dithering)(PEP-II)



When we shake the beam at around the peak of the luminosity, there appears twice of the frequency of the dithering frequency.

- Beam size feedback (KEKB horizontal)



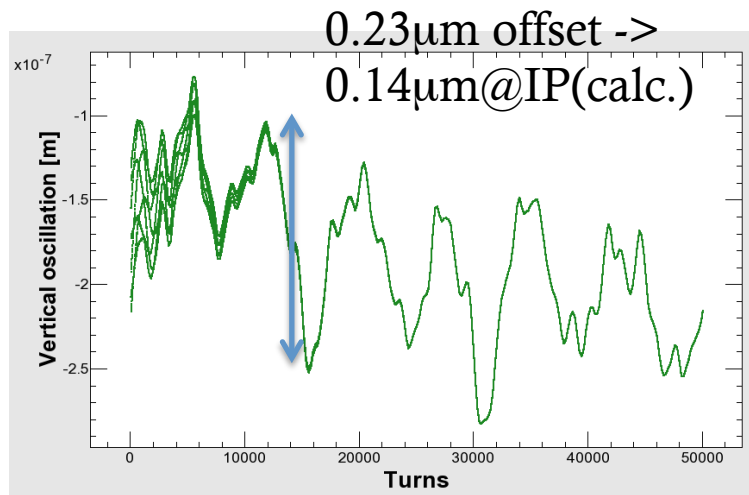
At KEKB before installation of crab cavities, the vertical beam of LER was used for the horizontal orbit feedback at IP.

QCS Vibration issues

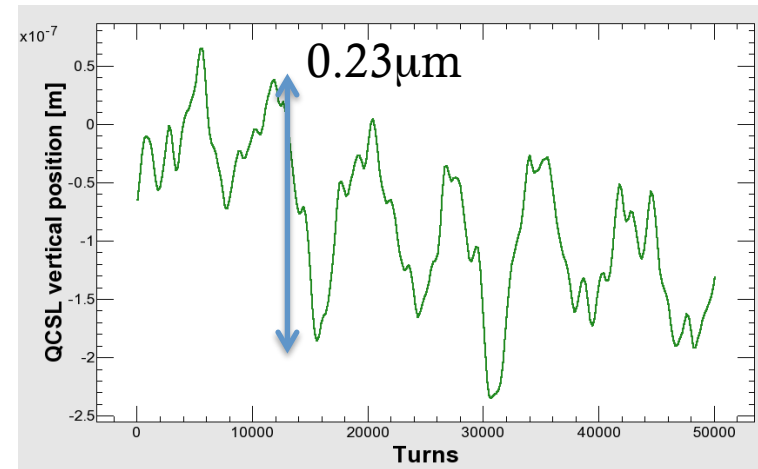
- The most serious source of orbit change at IP
- Recent progress
 - Coherency of vibration of QC1{RL}E and QC1{RL}P
 - Further damping of vibrations by using high damping materials
 - Suppression of orbit difference by orbit feedback system (H. Fukuma)

QCSL vertical position oscillation (measurement) and orbit change (tracking) : KEKB LER

Vertical orbit at IP
(simulation)



QCSL vertical position
(measurement)

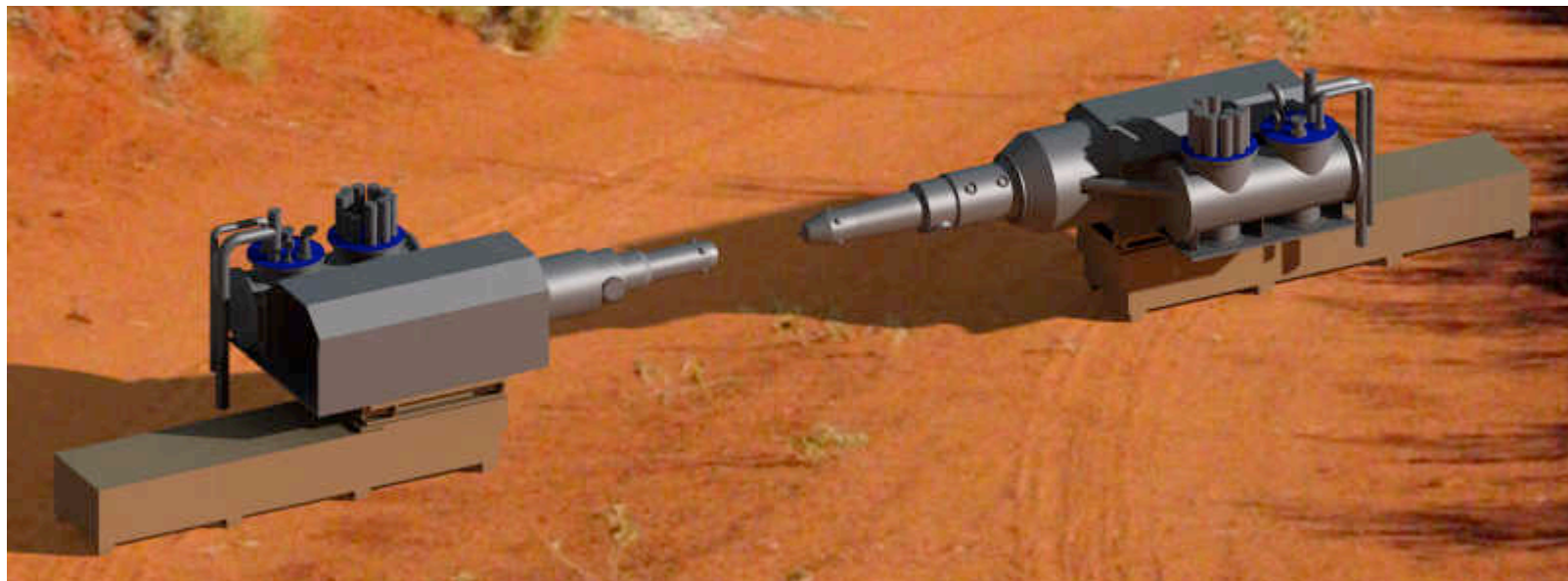
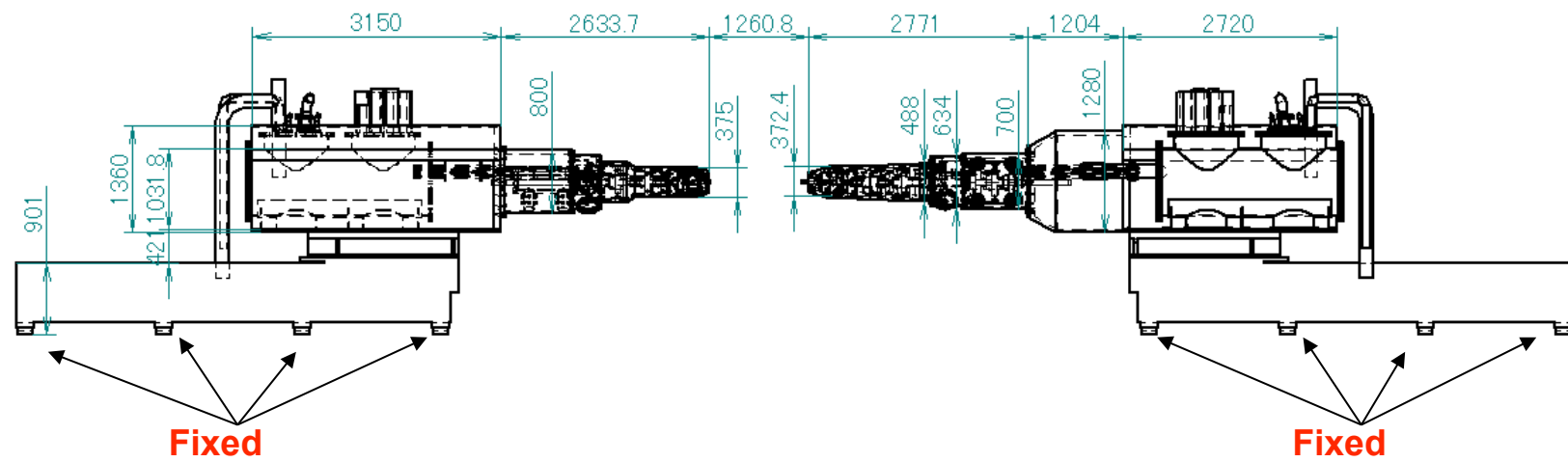


Simulation on vibrations of QCS magnets (H. Yamaoka)

- Simulation using ANSYS
 - Modal calculation
 - Resonant modes: ~26, 36, 39, 53 Hz
 - Oscillation amplitude (PSD (power spectrum density))
 - Input of simulation: Measured data on floor vibration
 - Coherency of vibrations of QC{12}RE and QC{12}RP or QC{12}LE and QC{12}LP
 - Coherency is very high
 - Further damping with high damping materials

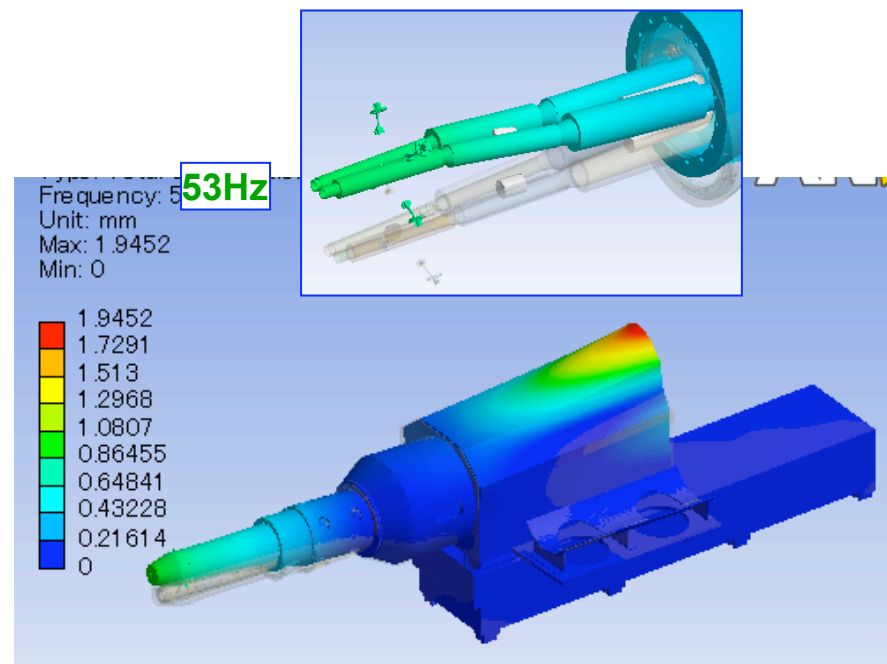
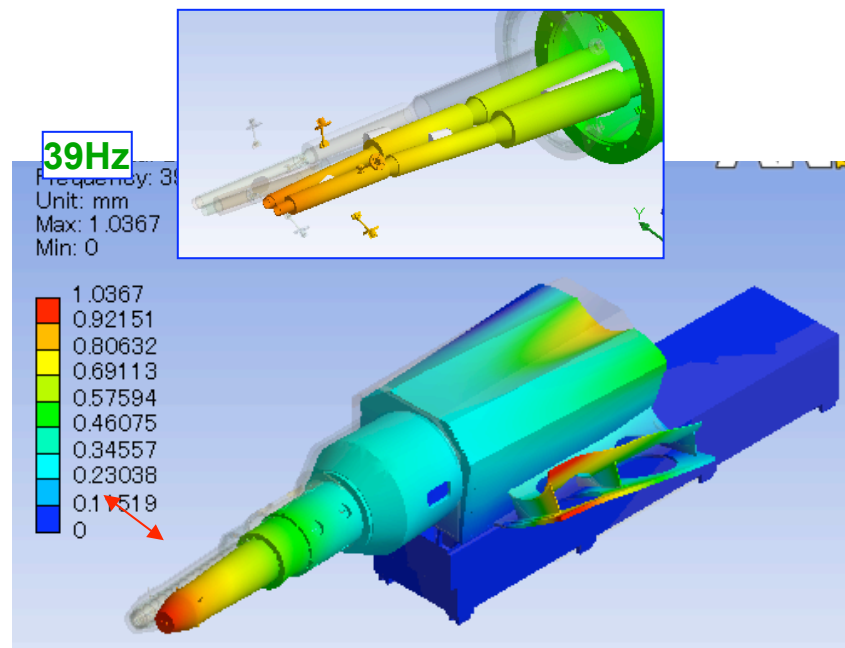
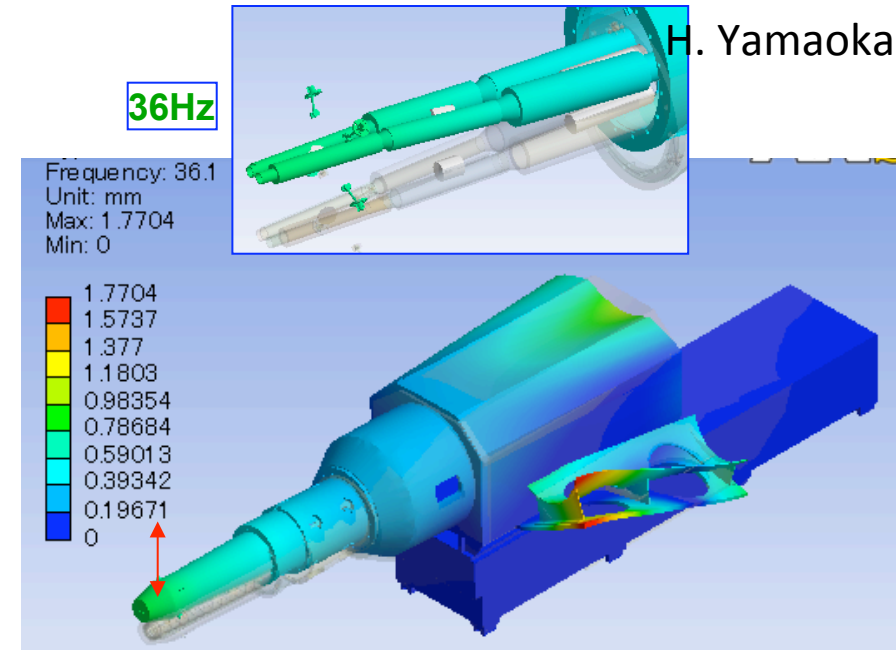
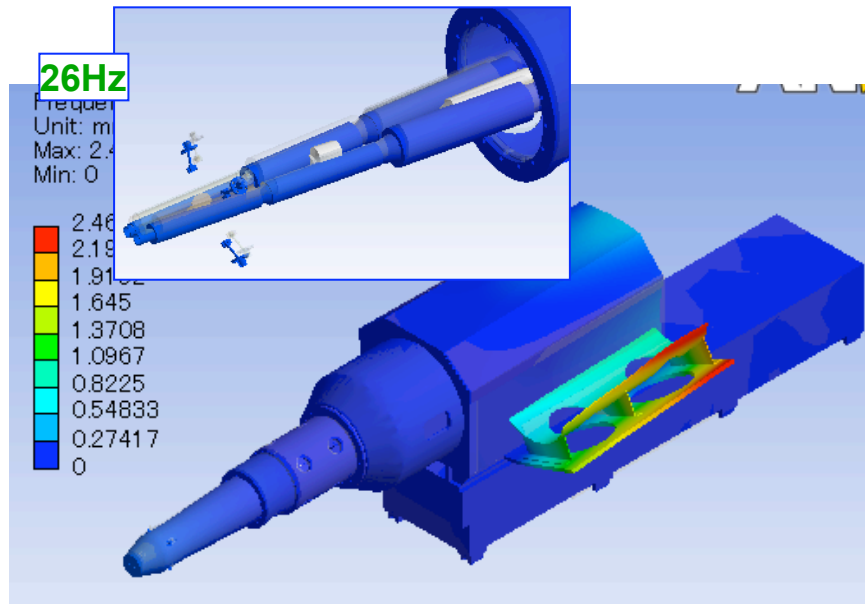
FEM model

H. Yamaoka



Modal calculation

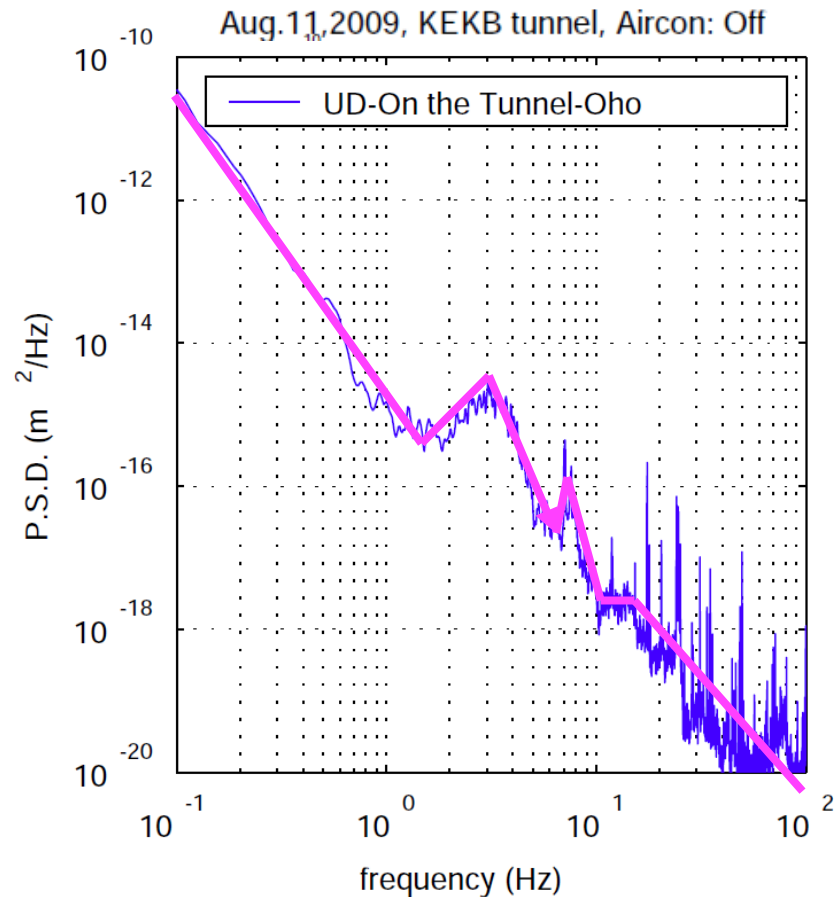
H. Yamaoka



P.S.D. (Power Spectrum Density) analysis

H. Yamaoka

In the vertical direction



Freq.(Hz) P.S.D.(m^2/Hz)

0.1 5e-11

1.5 5e-16

3.0 5e-15

6.5 5e-17

8.0 1e-16

10. 3e-18

16. 3e-18

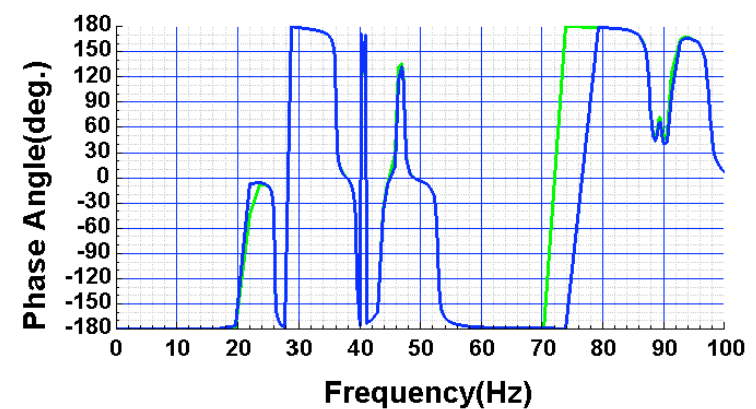
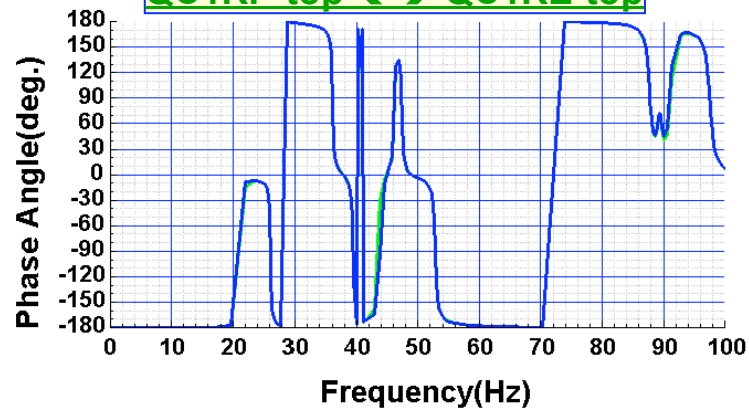
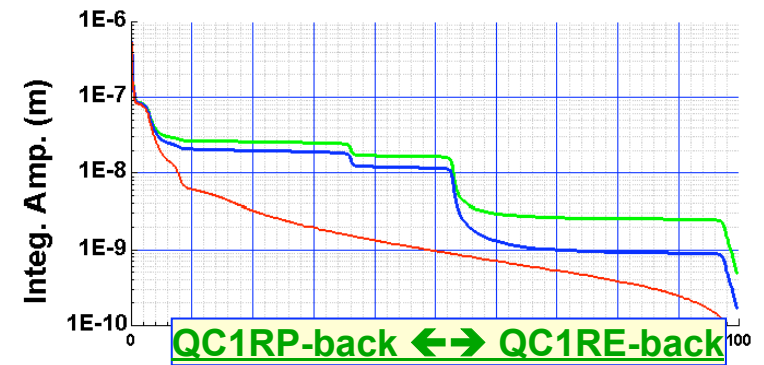
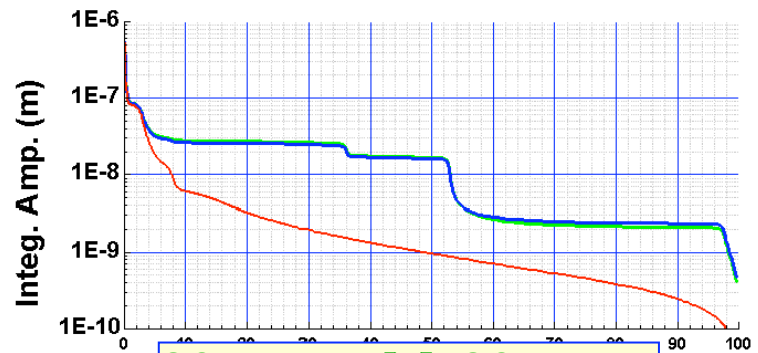
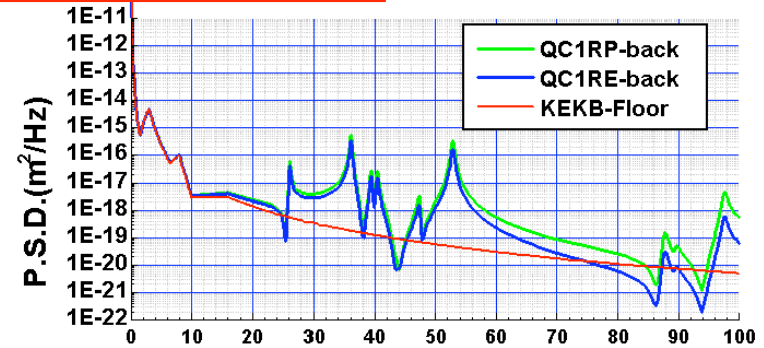
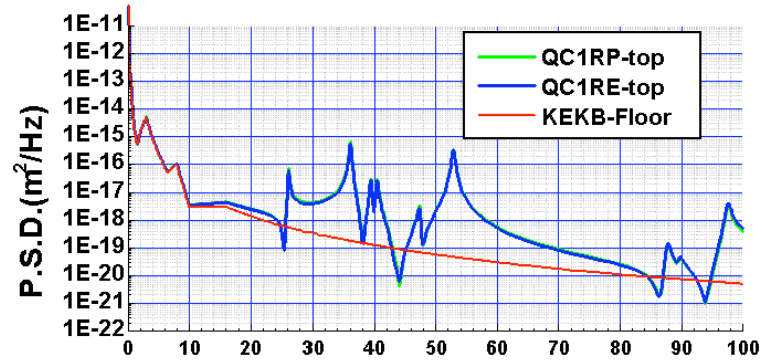
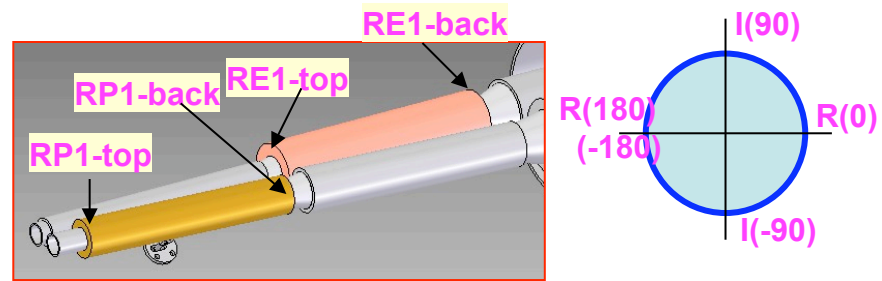
100. 5e-21

damping= 0.5%

Floor vibration: Input for the simulation

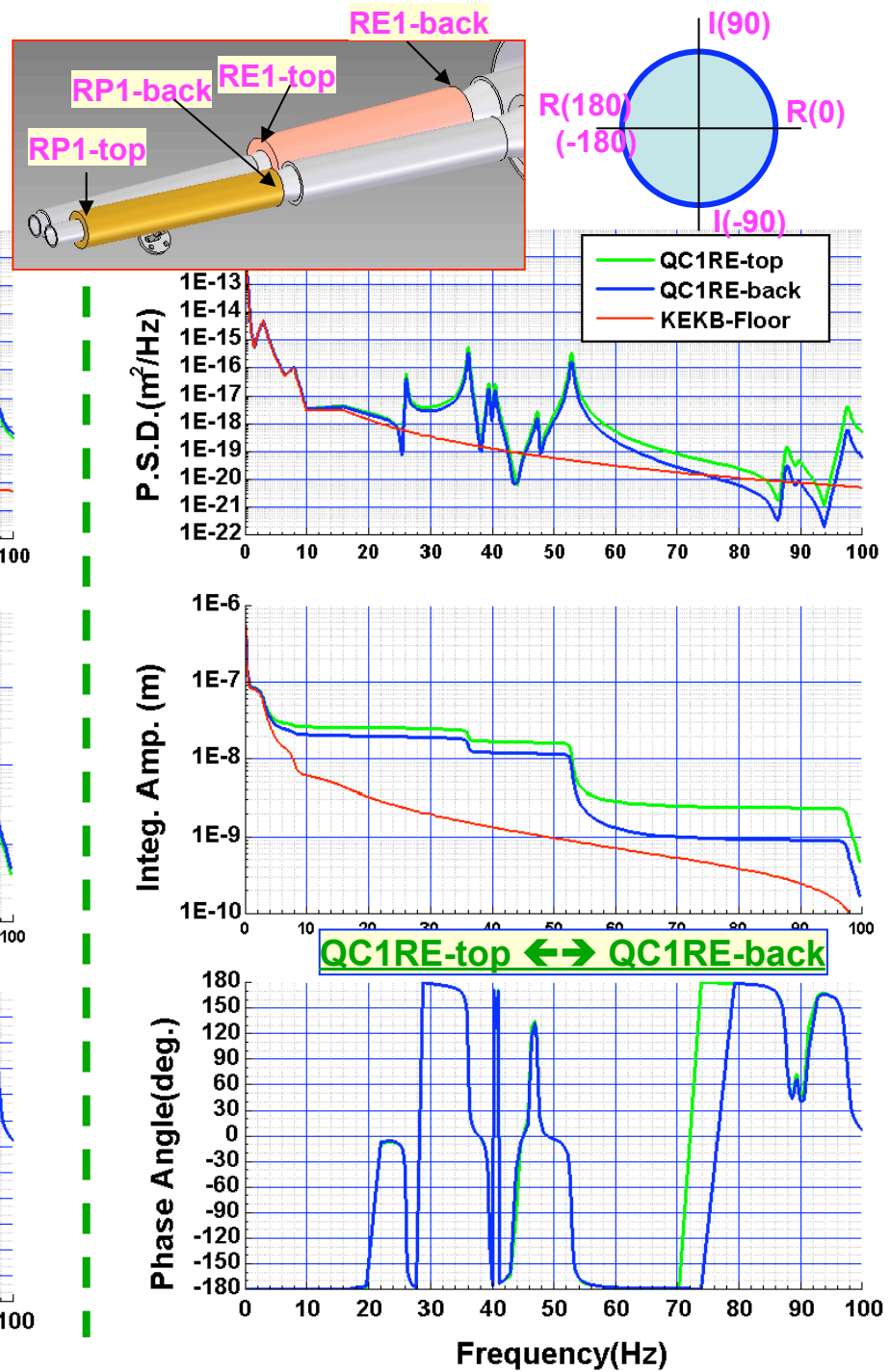
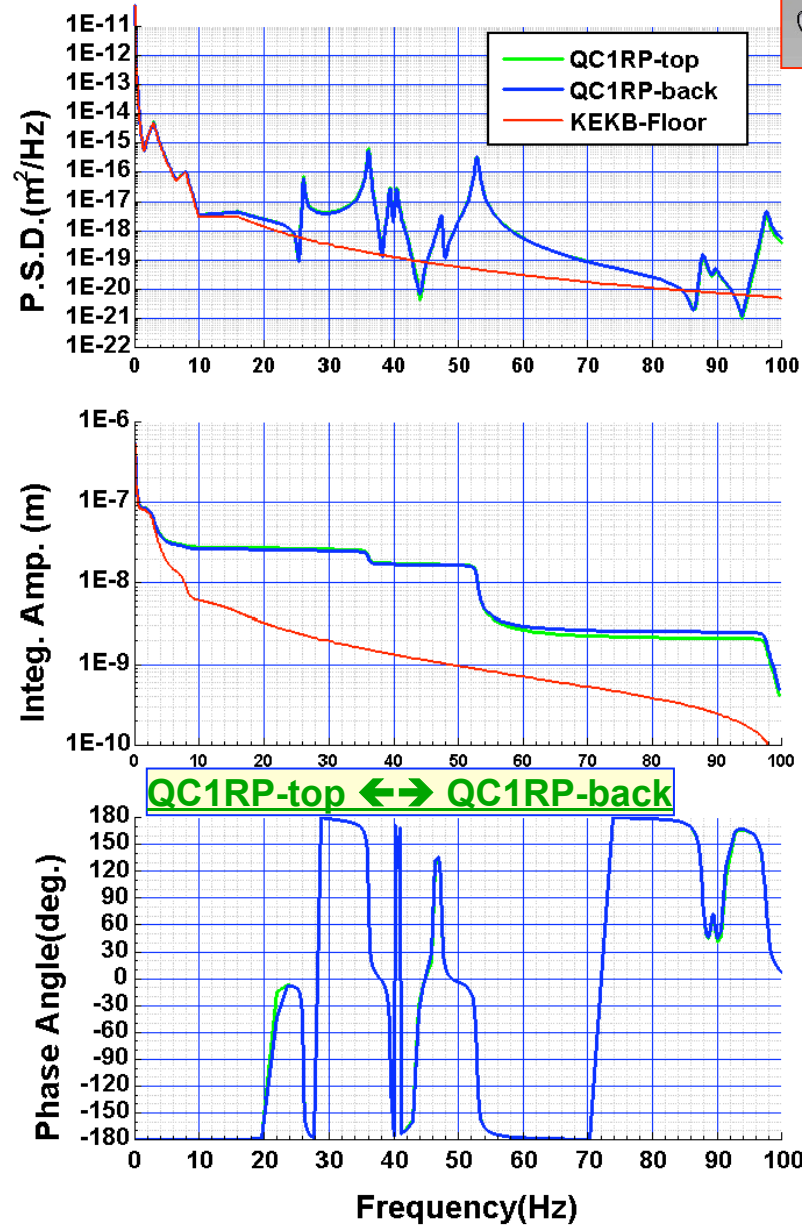
Results(Vertical direction)

H. Yamaoka



Results(Vertical direction)

H. Yamaoka



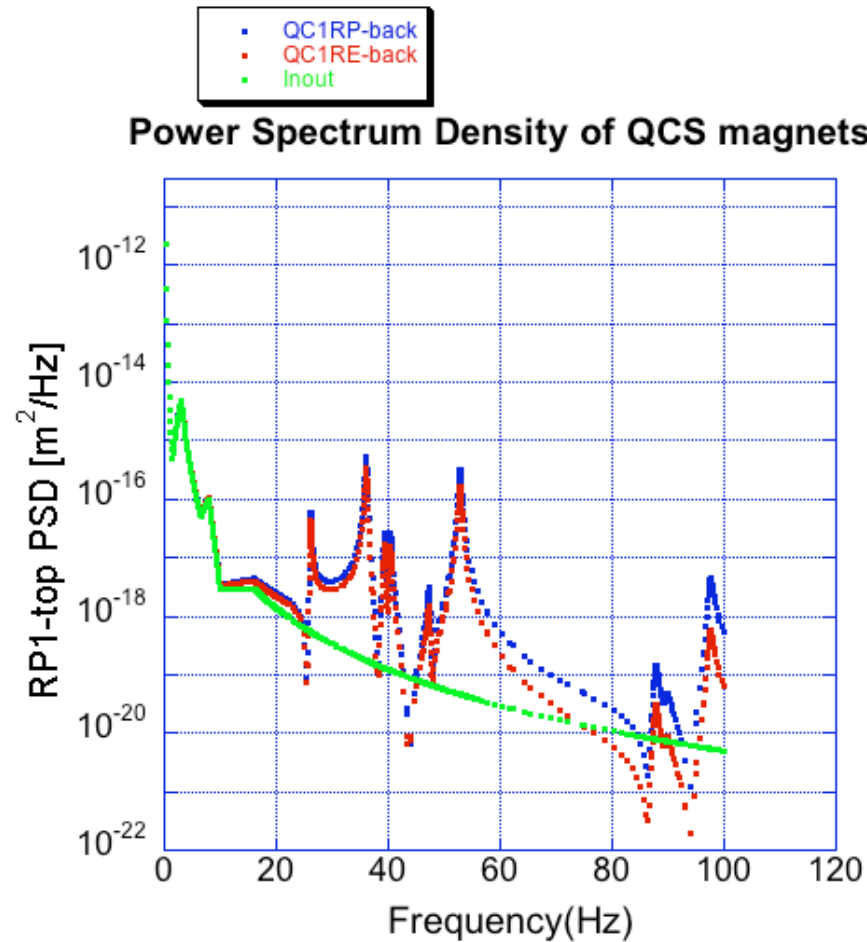
Orbit change at IP with 1 μm offset of QCS magnets

		K1 (/m)	Distance from IP [m]	β_Q [m]	β_{IP} [mm]	$\Delta\psi_y/2\pi$	COD@IP for 1 μm Q-offset [μm]
QC1L	LER	-1.717	0.912	2504.3	0.27	0.24995	-0.706
	HER	-1.142	1.390	5462.4	0.3	0.24997	-0.731
QC1R	LER	-1.712	0.912	2567.7	0.27	0.24996	-0.713
	HER	-1.070	1.430	5592.6	0.3	0.24997	-0.693
QC2L	LER	0.84161	1.9099	962.2	0.27	0.25004	0.2145
	HER	0.65023	2.6799	1923.3	0.3	0.25030	0.2470
QC2R	LER	0.83924	1.9760	924.6	0.27	0.25005	0.2097
	HER	0.55577	2.9449	1806.9	0.3	0.25004	0.2046

$$\text{COD} \quad \Delta y = \frac{1}{2 \sin \pi \nu} \sqrt{\beta_Q \beta_{IP}} \cos(\pi \nu - |\Delta \psi|) \vartheta$$

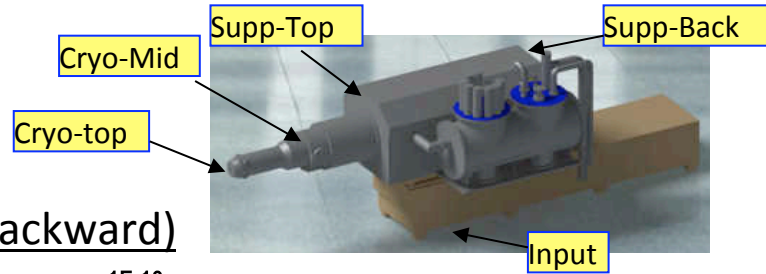
If QCS magnets for LER & HER move coherently, orbit difference of the two beam becomes much smaller (1/10 ~ 1/20) than non-coherent case.

Time domain vibration data to reproduce PSD from Yamaoka

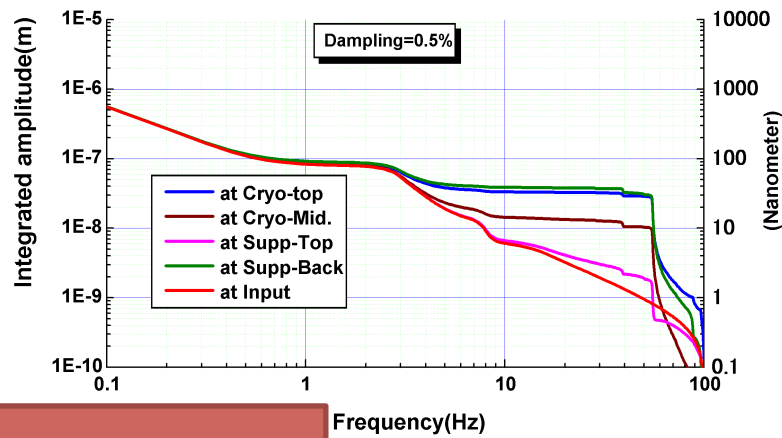
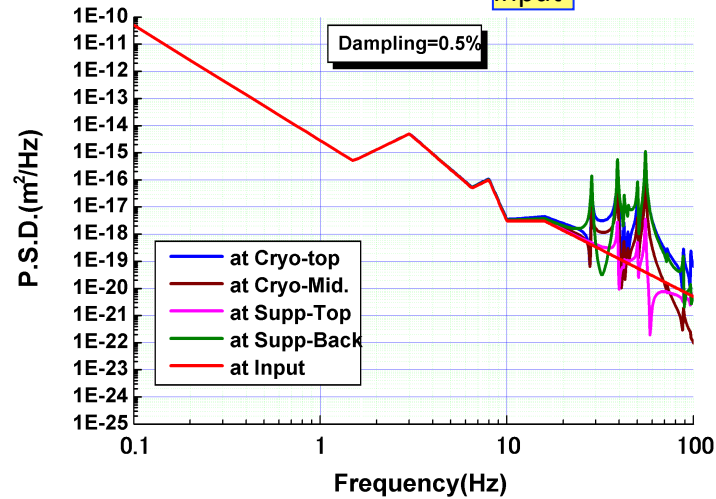


- To make a mode to reproduce the floor vibration (Ornstein-Uhlenbeck process)
- 3 resonant modes (3, 36 and 53Hz) are created.

Results(Vertical direction)

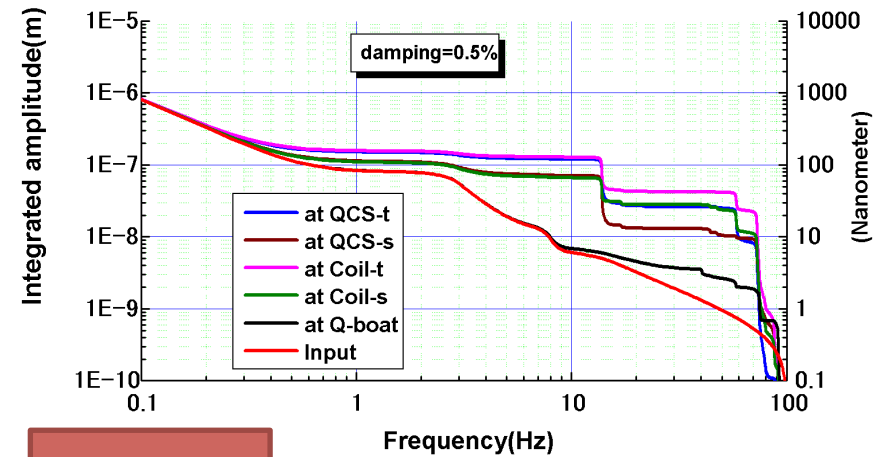
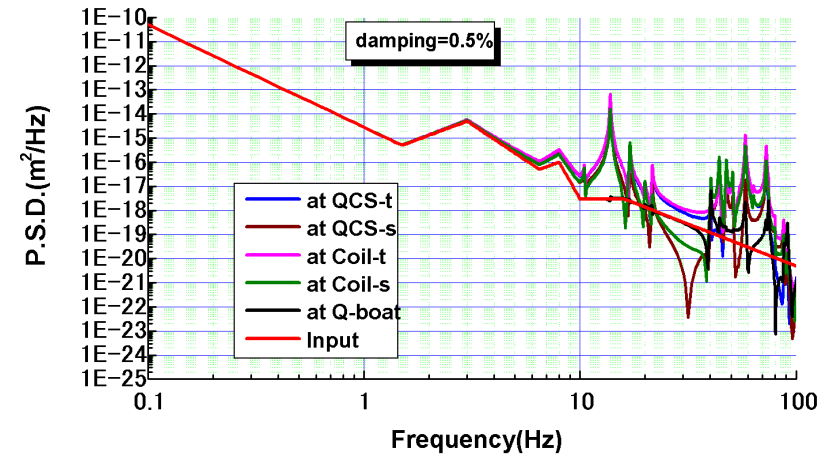
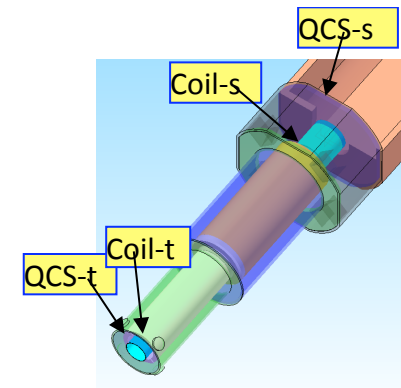


(Backward)



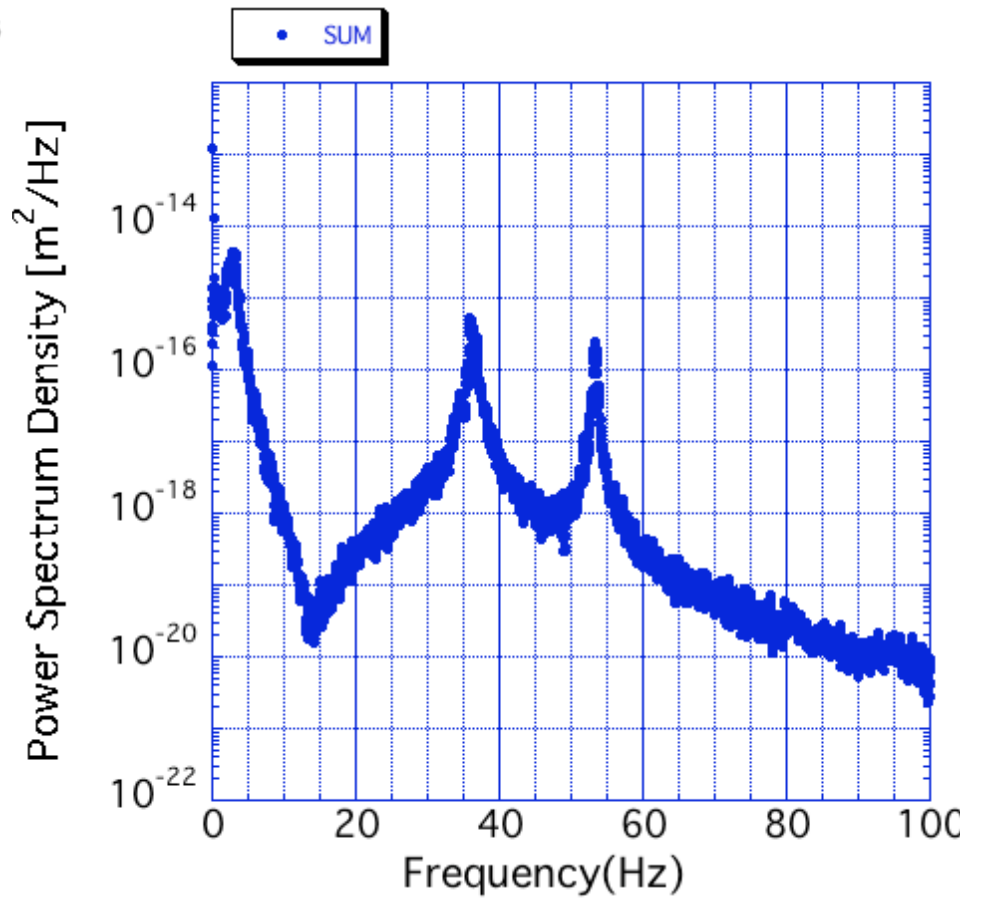
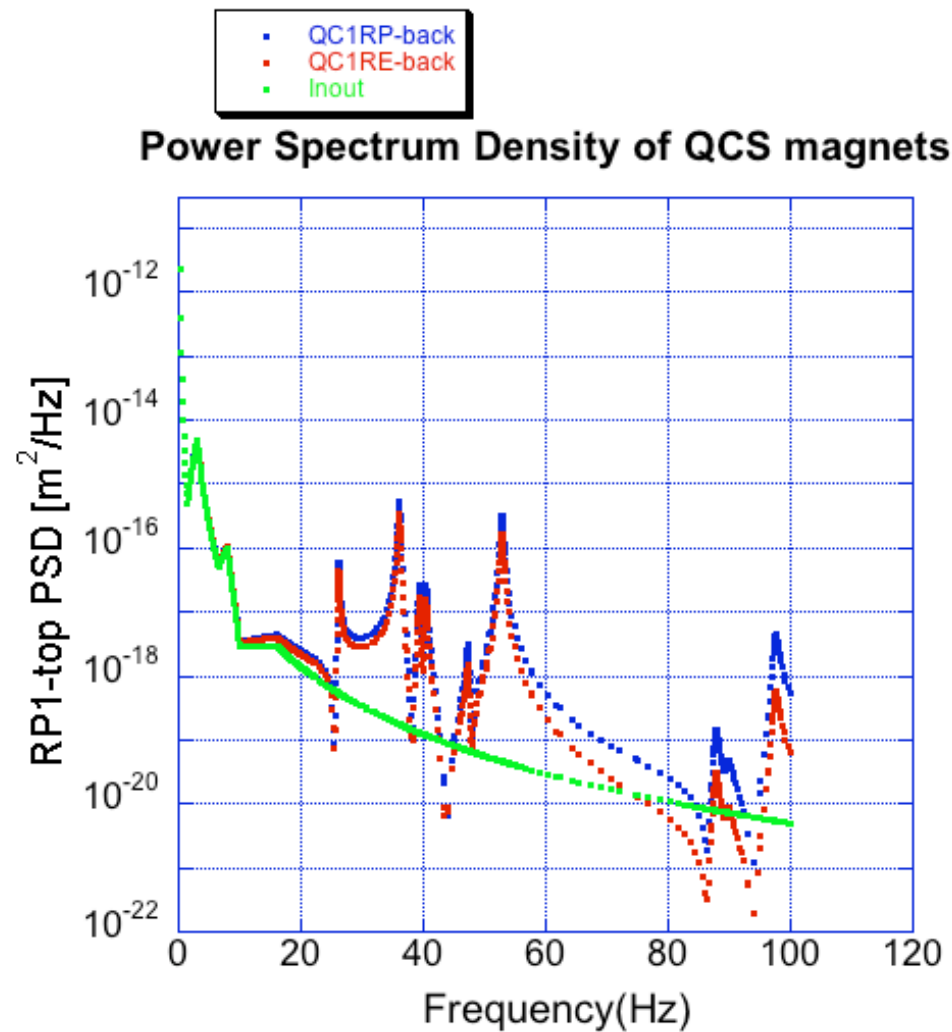
SuperKEKB

H. Yamaoka



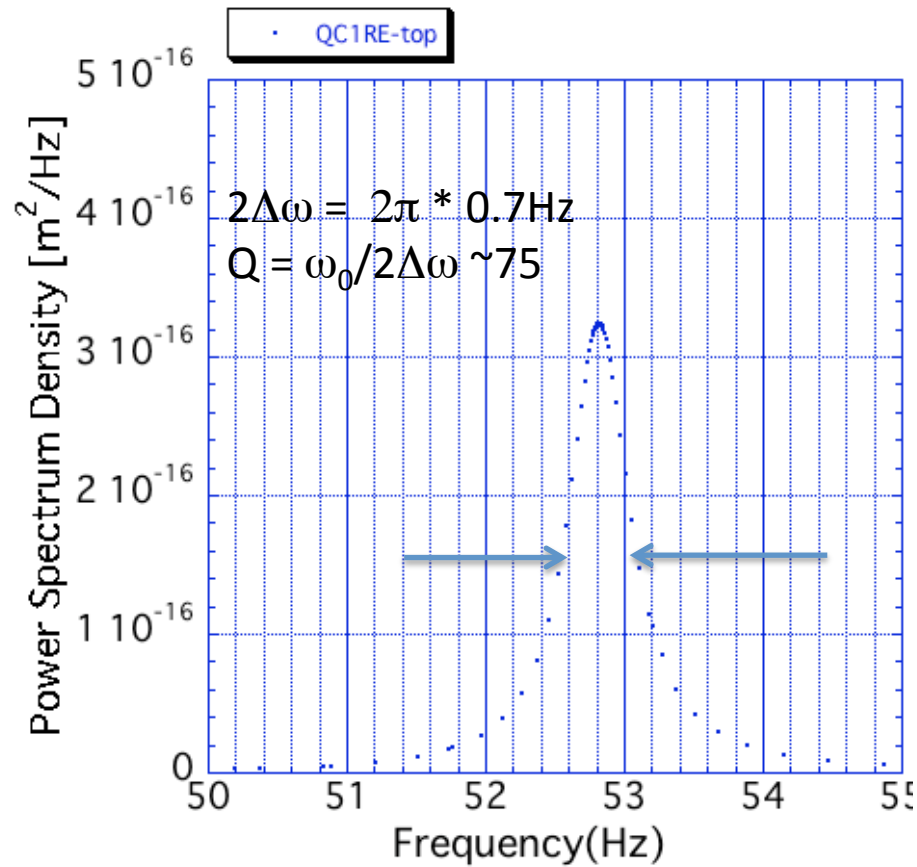
KEKB

Reproduced PSD

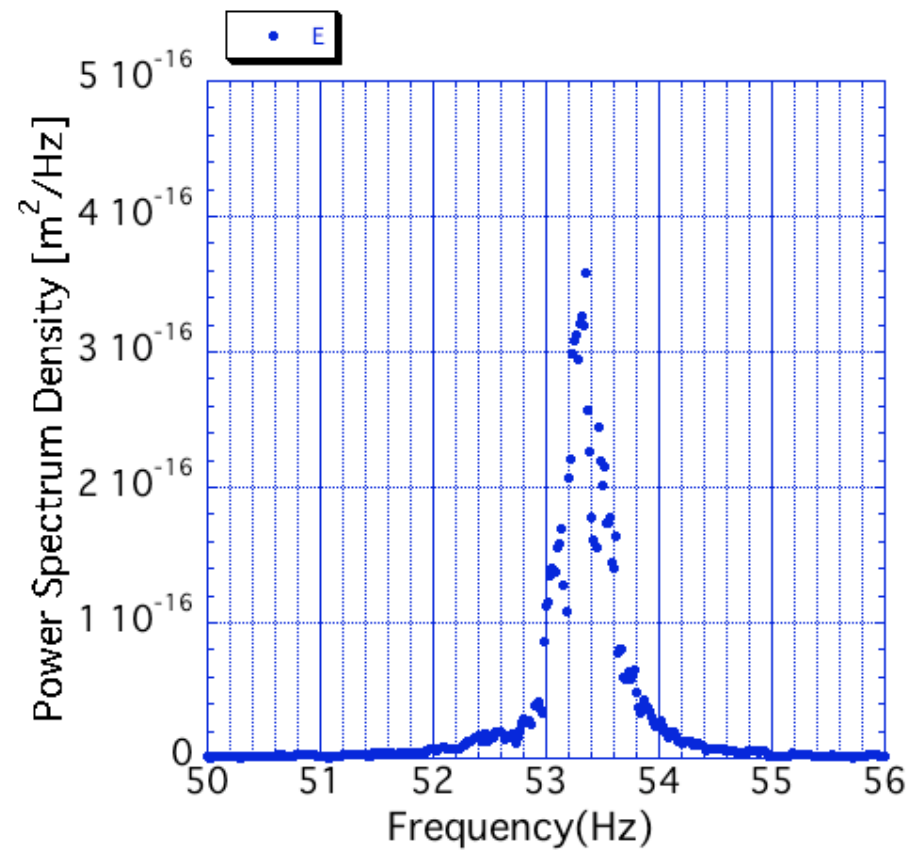


Resonance at ~53Hz

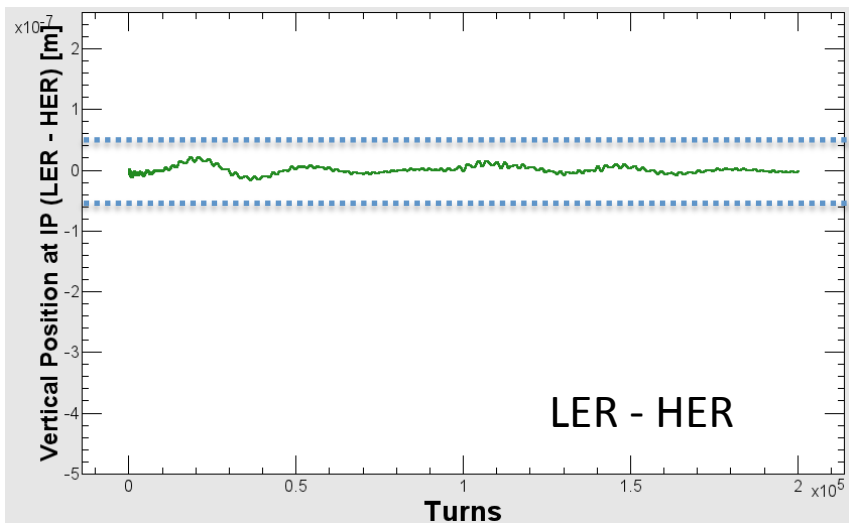
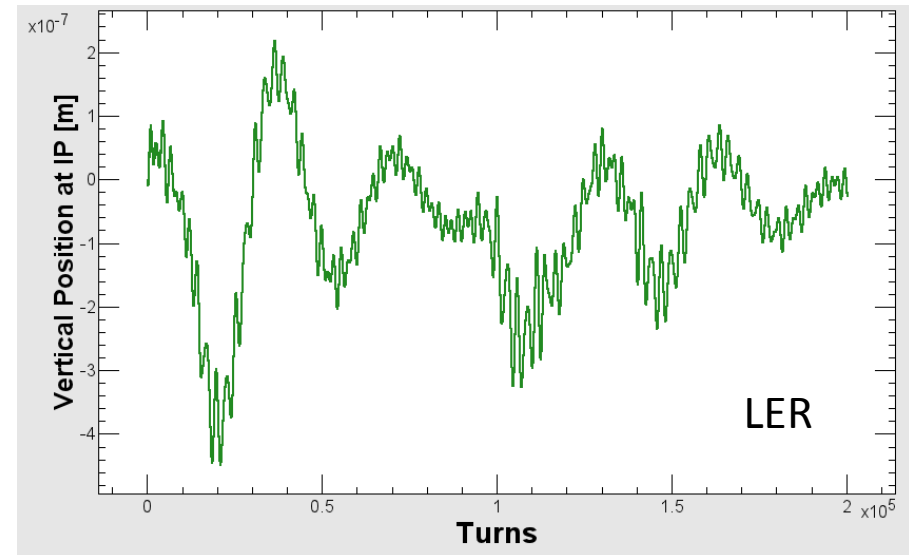
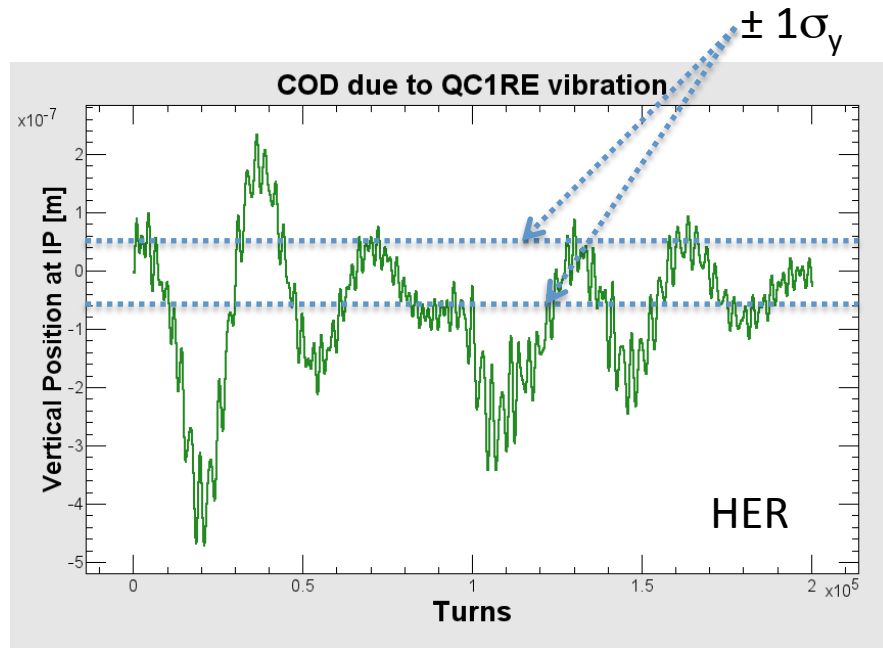
PSD from H. Yamaoka



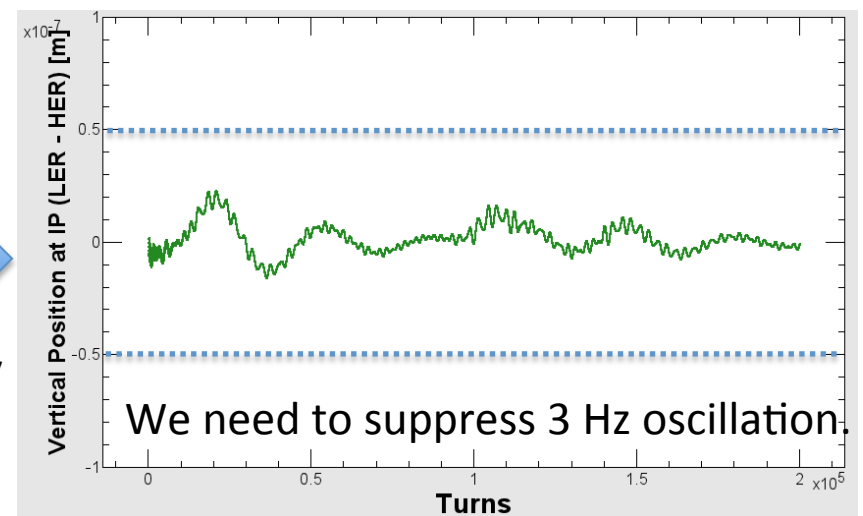
Reproduced by Funakoshi



COD simulation due to QC1R vibration in case that QC1RE and QC1RP move in the same way

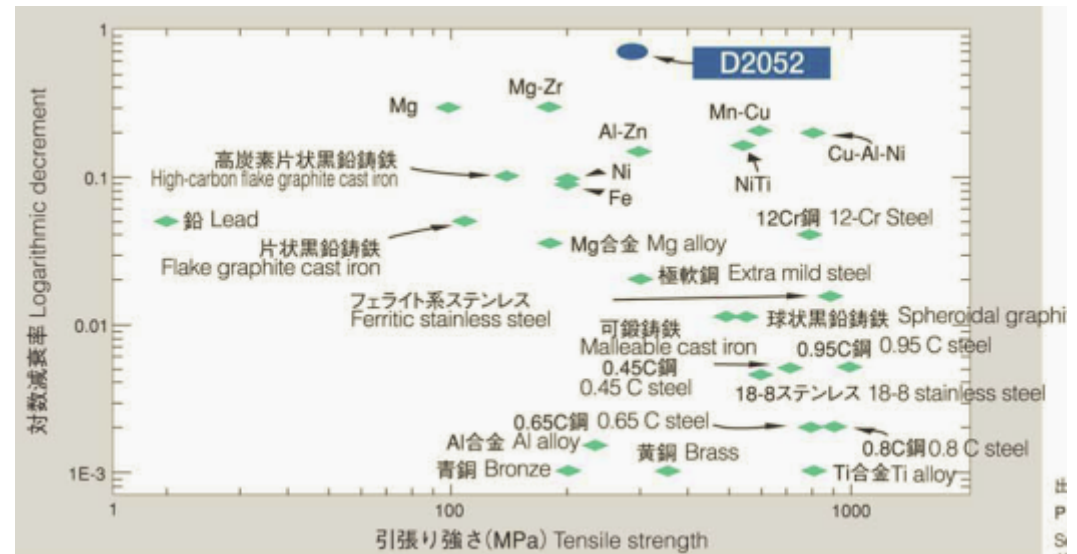
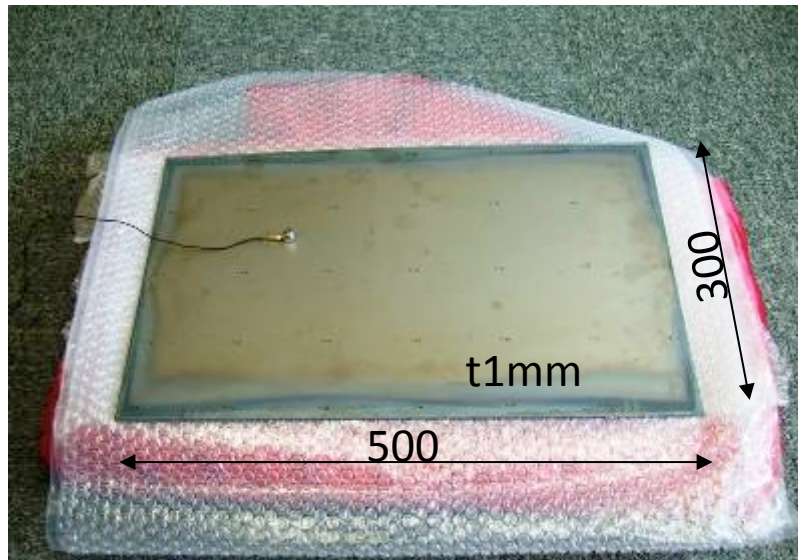


Magnify



High Damping Material: D2052

H. Yamaoka



代表的な化学成分 Typical chemical composition

Mn	Cu	Ni	Fe	単位 Unit
Bal.	22.4	5.2	2.0	wt%
Bal.	20.0	5.0	2.0	at%

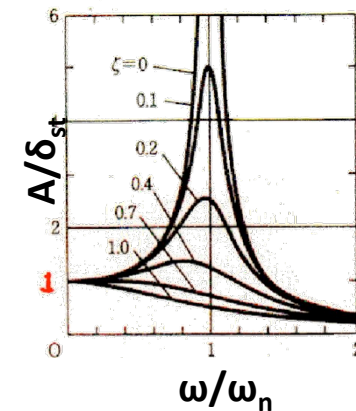
Mn-base damping alloy

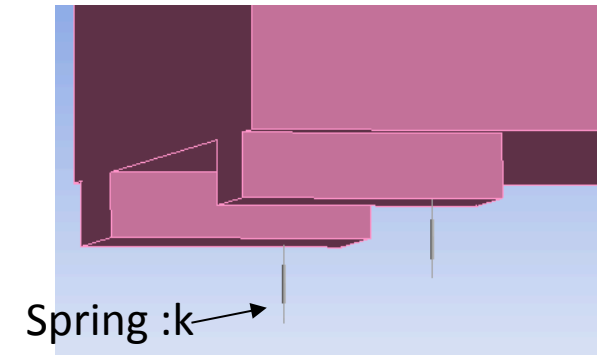
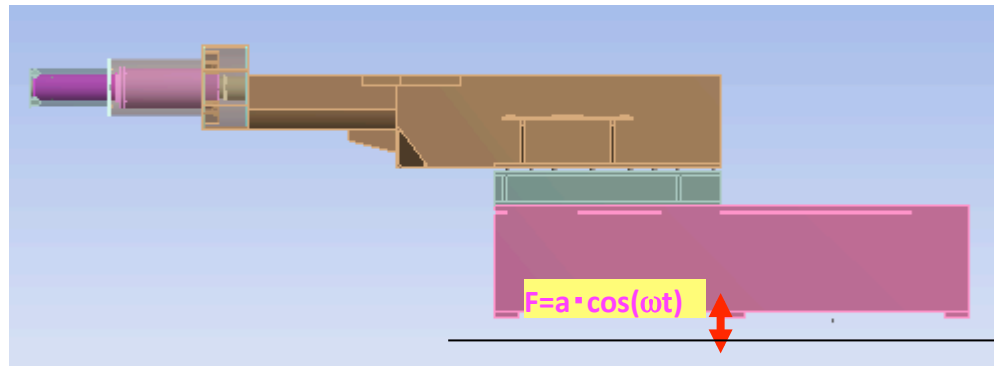
主な物性値 Typical properties

物性 Property	値 Value	近い元素 Approximate element
ヤング率 Young's modulus	80 GPa (300K)	Al, Ag, Cd
熱伝導率 Heat conductivity	10 W/(m·K) (300K)	Ti, Sb, Pb, Bi
比熱 Specific heat	512.7 J/(kg·K) (300K)	Ti, Fe, Cr
熱膨張率 Coefficient of thermal expansion	$22.4 \times 10^{-6}/K$ (300K)	Al, Ag, Sn, Cu
密度 Density	$7.25 \times 10^3 \text{kg/m}^3$	Fe, Mn
硬さ Vicker's hardness	120~140	

機械的強度 Mechanical strength

	引張強さ Tensile strength	耐力 (0.2%) Yield strength	伸び Elongation	絞り Reduction of area	疲労強度 ($\times 10^7$ 回) Fatigue strength ($\times 10^7$ times)
標準材 Standard material	530MPa	265MPa	40%	61%	125MPa





$$F = 1 \times 10^4 \text{ N}$$

$$k = 2 \times 10^5 \text{ N/mm}$$

Materials (w/o damping material)

Cryostat: SUS

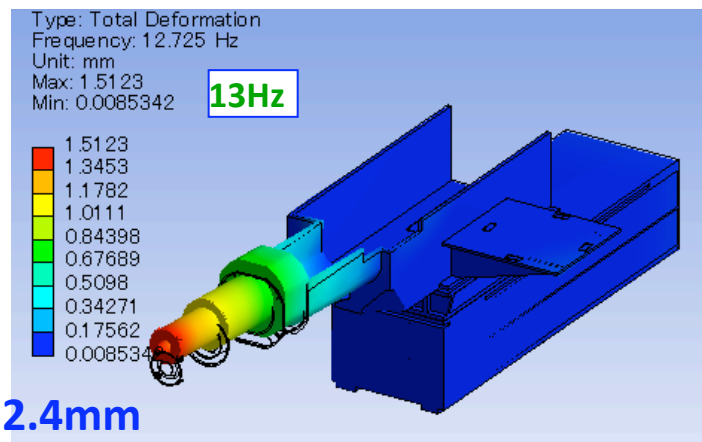
Coil: Cu

Supp.-rod: Ti-alloy

QCS table: SS400

damping = 0.5%

→ Response displacement: 12.4mm
eigen-frequency: 13Hz



Materials

Cryostat: SUS

Coil: Cu

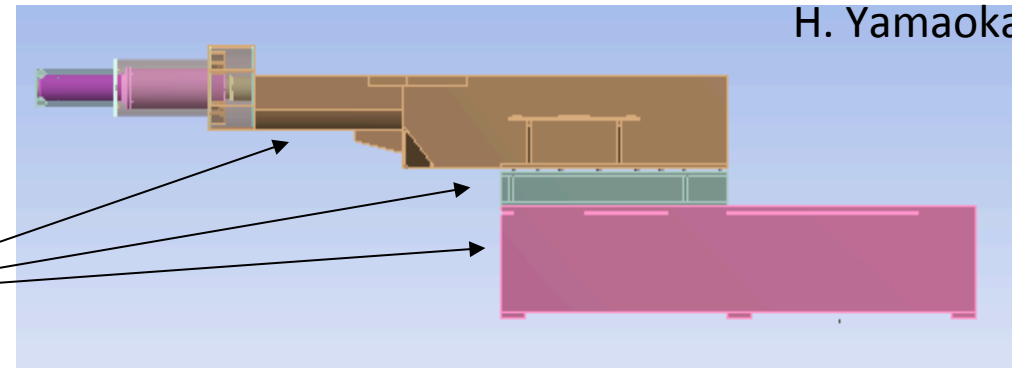
Supp.-rod: Ti-alloy

QCS tables: damping material

damping= 5%

bolts: damping material

➔ Response displacement: 3.2mm(damping: 74%)
 eigen-frequency: 9Hz

Materials

Cryostat: SUS

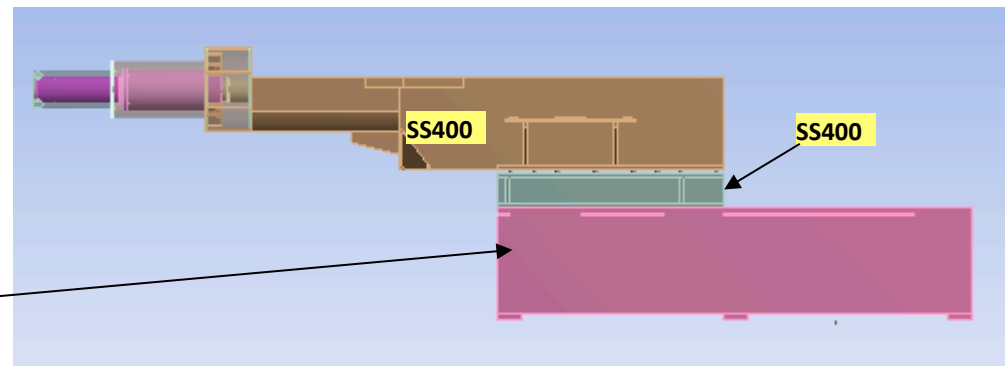
Coil: Cu

Supp.-rod: Ti-alloy

QCS table: damping material

bolts: damping material

➔ Response displacement: 6.0mm(damping: 51%)
 eigen-frequency: 11.6Hz



Materials

Cryostat: SUS

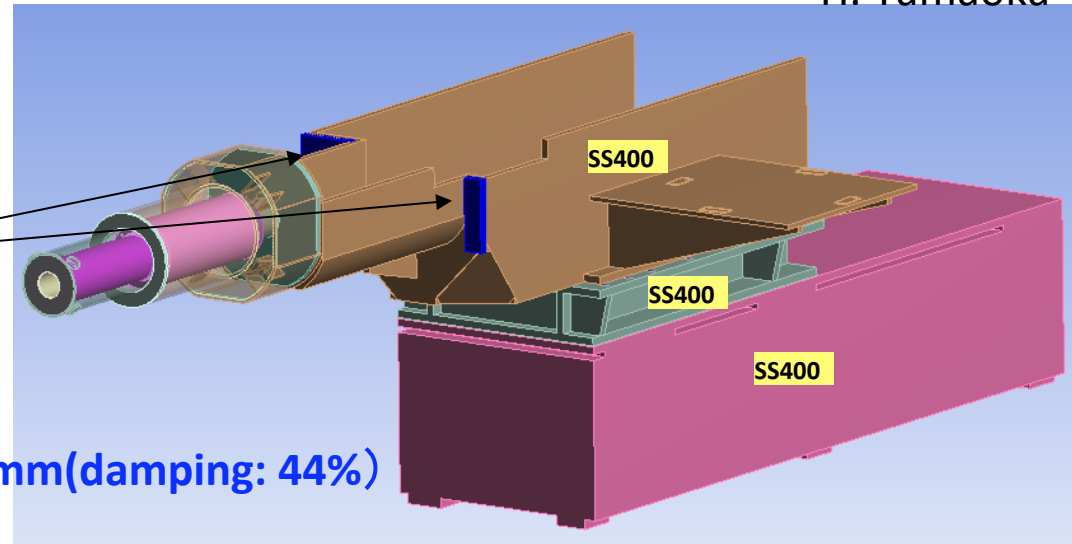
Coil: Cu

Supp.-rod: Ti-alloy

QCS table: damping material
welding (t45mm)

bolts: damping material

→ Response displacement: 6.9mm(damping: 44%)
eigen-frequency: 13.7Hz



This case seems realistic.

Materials

Cryostat: SUS

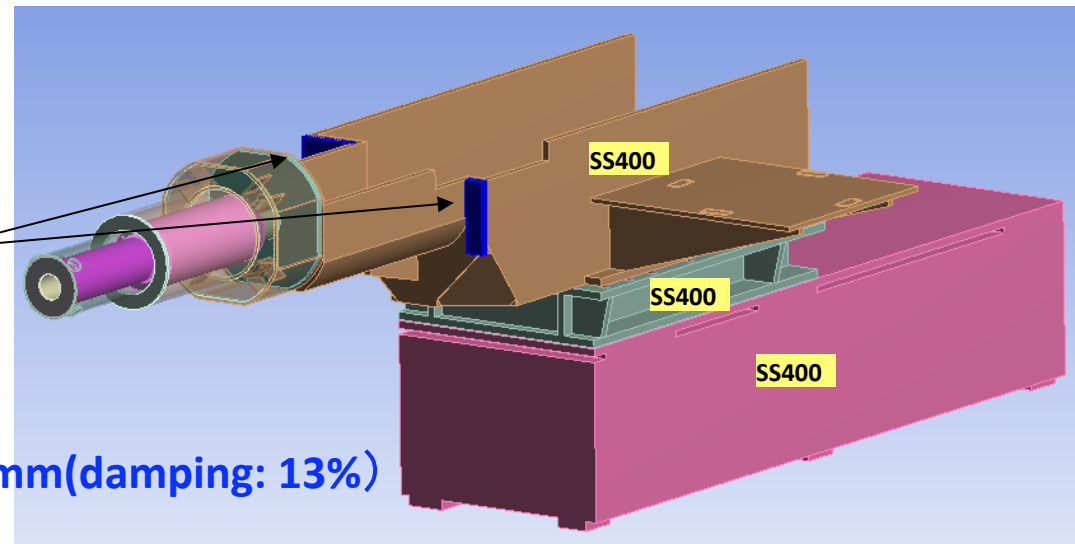
Coil: Cu

Supp.-rod: Ti-alloy

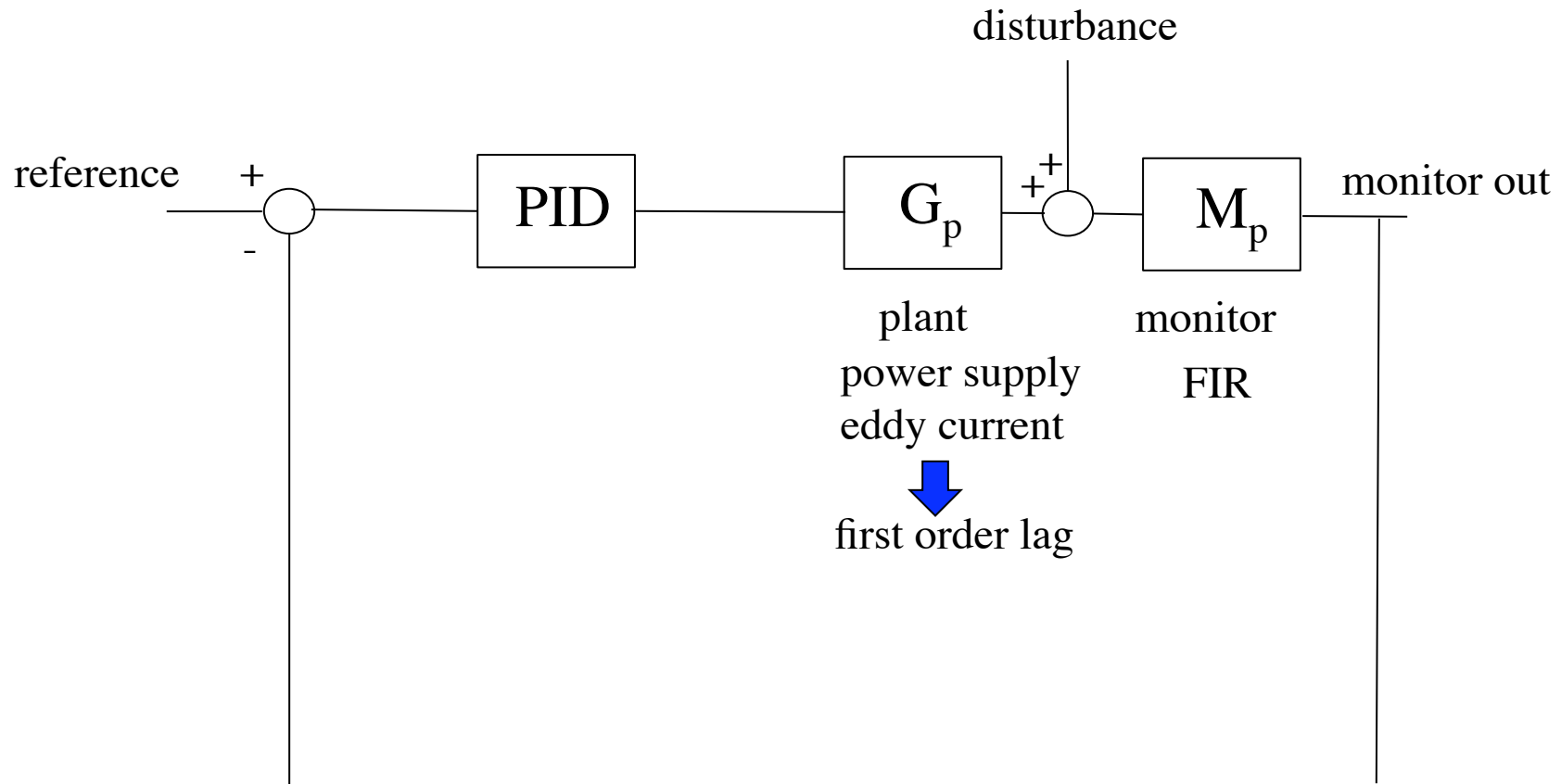
QCS table: steel instead of damping
material welding(t45mm)

bolts: damping material

→ Response displacement: 10.8mm(damping: 13%)
eigen-frequency: 13.7Hz

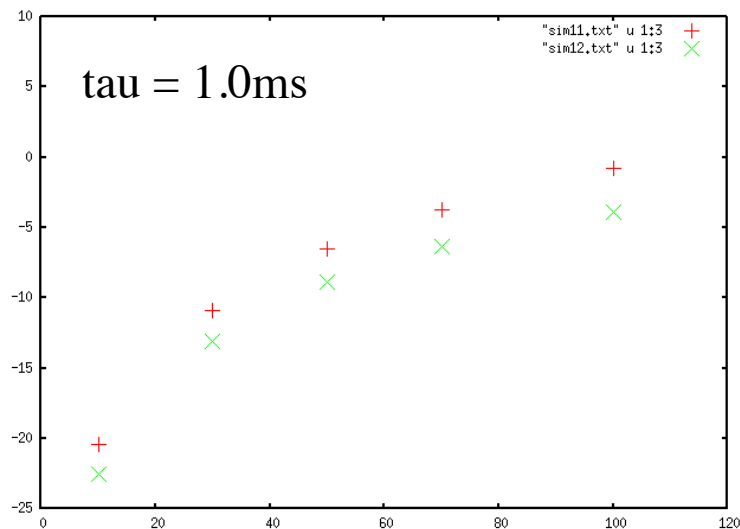
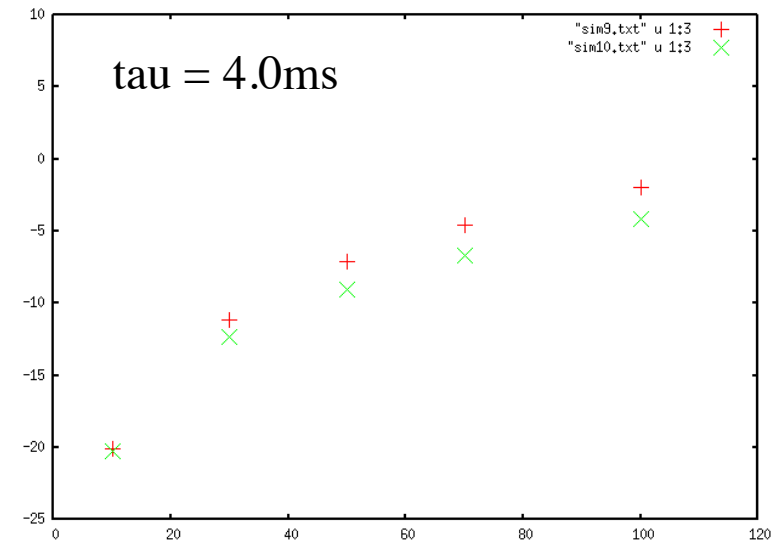
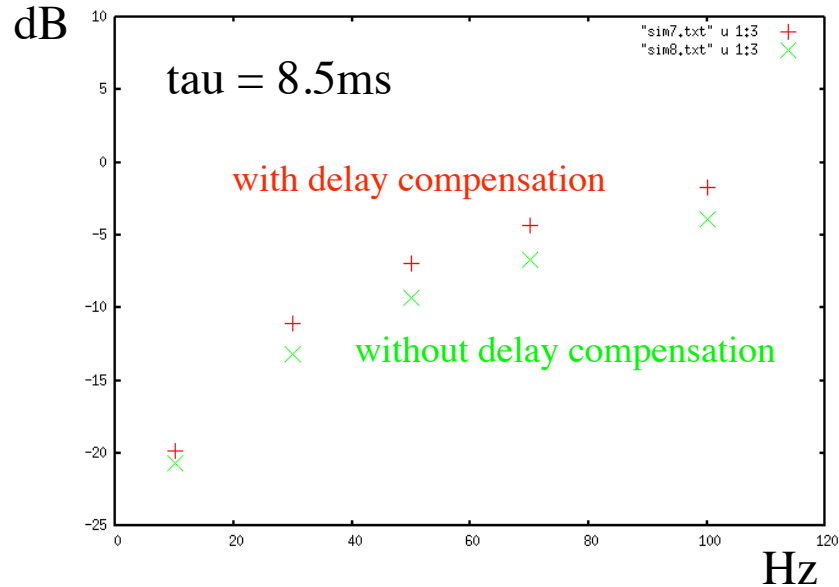


Orbit Feedback System



Analysis of FB system by H. Fukuma

group delay = 5 samples (1.1ms)



Disturbance suppression is weaker
with delay compensation.

If group delay is reduced to 1ms, **rejection gain at 10/100Hz is -22/-5 dB**, and gain is almost not dependent on time constant of the plant.

Tau is the time constant of the plant coming from eddy current and delay in power supply etc.

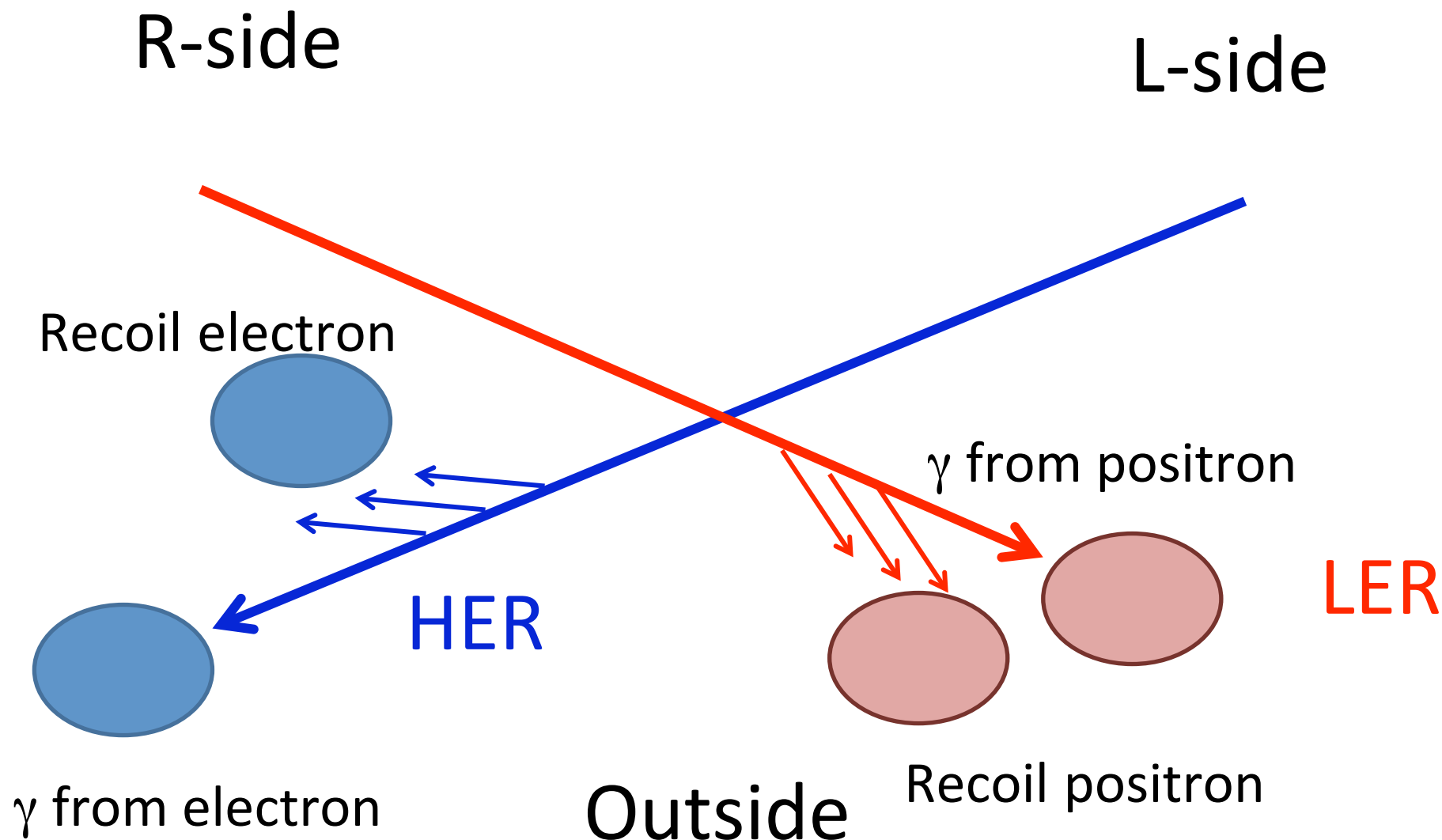
Horizontal orbit feedback

- Difficulty to develop FB based on the beam-beam deflection like the vertical case
 - Small ξ_x
 - $\xi_x \sim 0.0028(e+), 0.0017(e-)$
 - Two sources of horizontal beam-beam kick
 - Horizontal offset and shift of collision timing
- Maybe we need a different method for the Hor. feedback.
 - Luminosity feedback (dithering) (like PEP-II)
 - Beam size feedback (like KEKB Hor. feedback before crab)
- Effect of horizontal offset with crab waist scheme
 - Due to Hor. offset, the two beams collide at the position which is shifted from the waist point.
 - The crab waist seems to compensate this shift of waist.
 - However, the situation becomes worse with the crab waist, since we have to keep the both beams at the design collision point with crab waist scheme.
- Feedback speed
 - Orbit change at IP due to fast vibration of IR quads is small. We do not need very fast feedback.

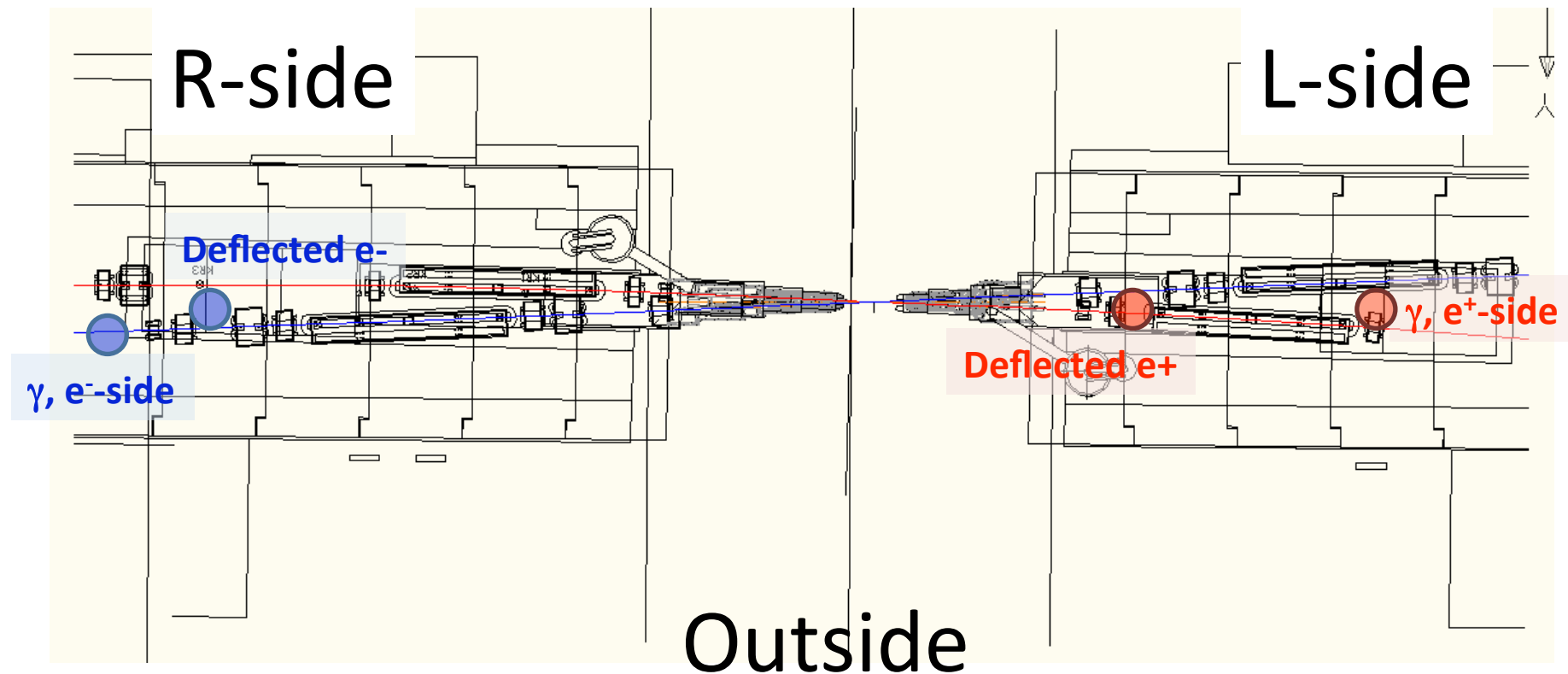
Dithering for Horizontal FB

- We have started to consider the dithering system based on experience at PEP-II.
- Conceptual design
 - Monitoring
 - Fast luminosity monitor (ZDLM)
 - Detect gamma-ray or lost particles from radiative Bhabha scattering
 - Magnets for dithering
 - Dithering frequency: $60 < \text{Freq.} < 100\text{Hz}$
 - Amplitude of dithering: $\sim < 0.5\sigma_x$ -> steering kick angle: $\sim < 5\mu\text{rad}$
 - Steering magnets: magnets with air core coils
 - Electronics
 - Lock-in amp (PEP-II) -> spectrum analyzer
 - Steering magnets for orbit correction
 - Use usual DC steering magnets for FB

Where are the signals?



Possible locations

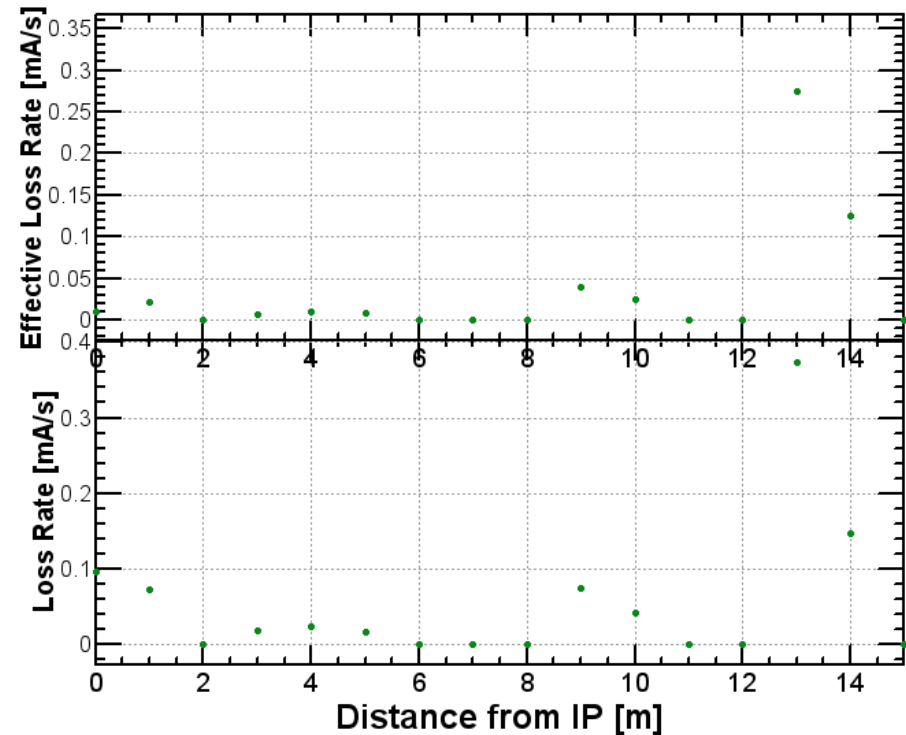
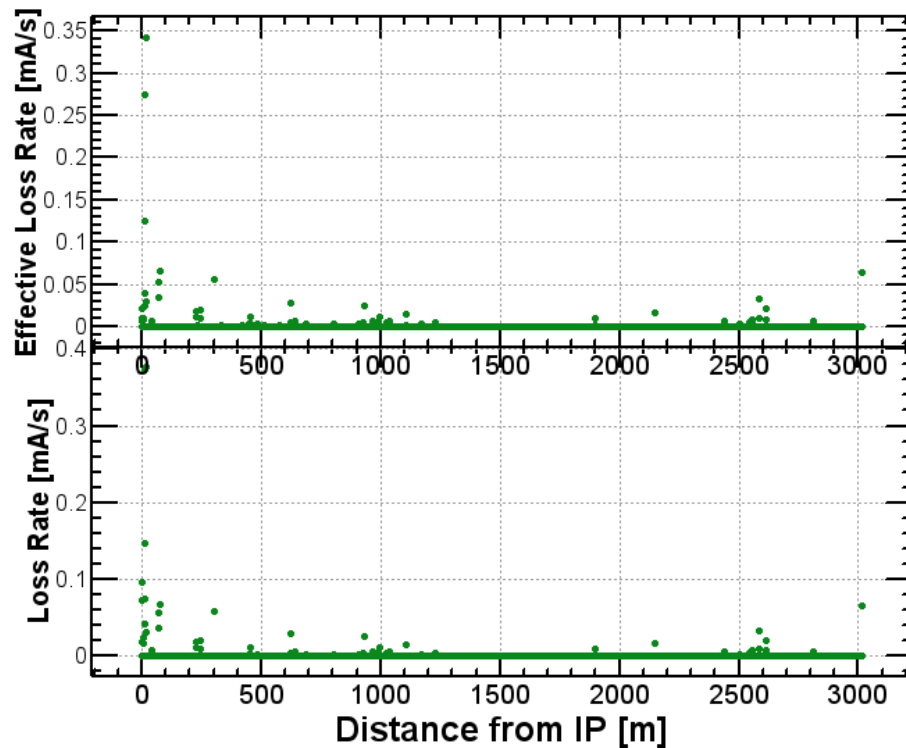


Possible problems:

- Material quantity of the beam chamber in r.l.

- Undesirable sensitivity to angle and position/size of the beams at IP

Beam loss simulation from radiative Bhabha: LER Loss Position & Rate



Loss rate: R_{Loss} [mA/s] = $1000N$ [partices/s] e f_0

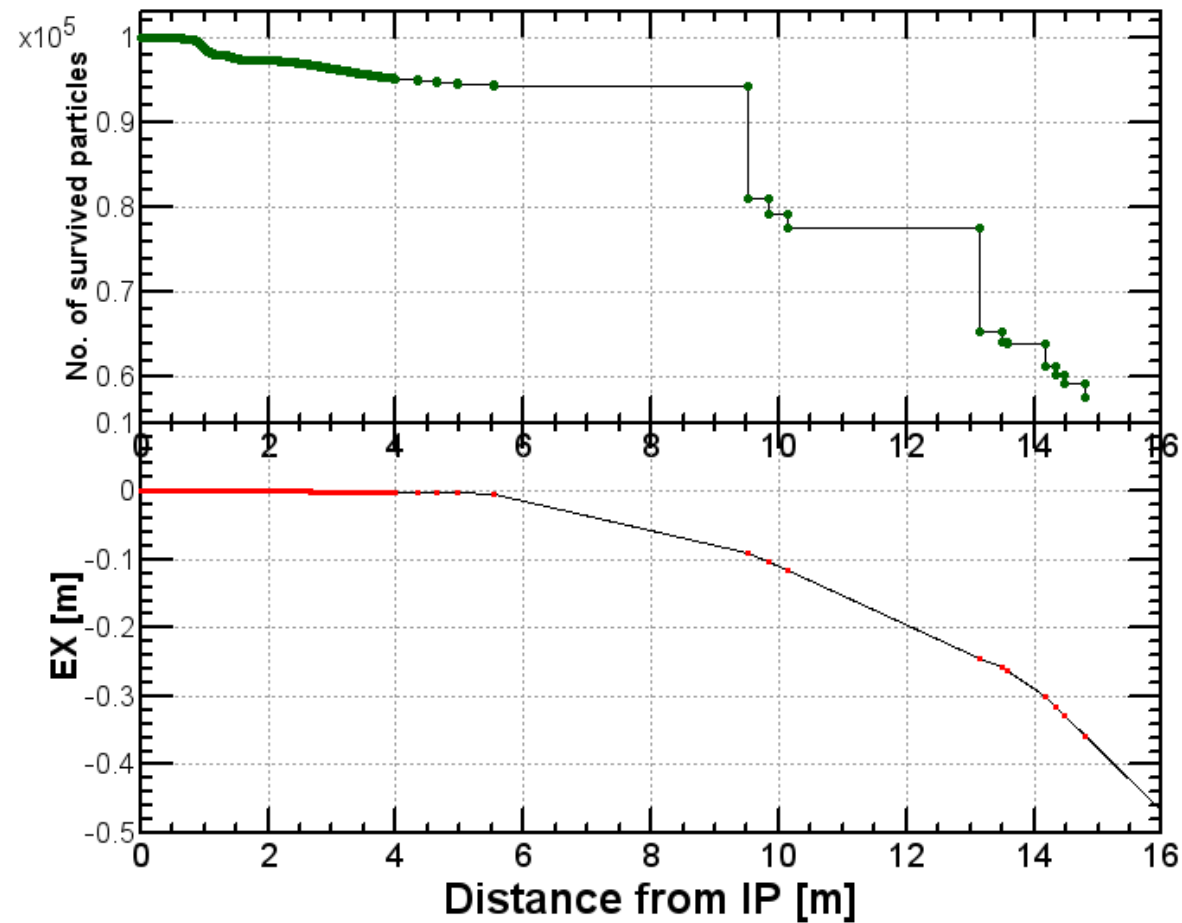
$e = 1.602 \times 10^{-19}$ [C]

$f_0 \cong 100$ [kHz]

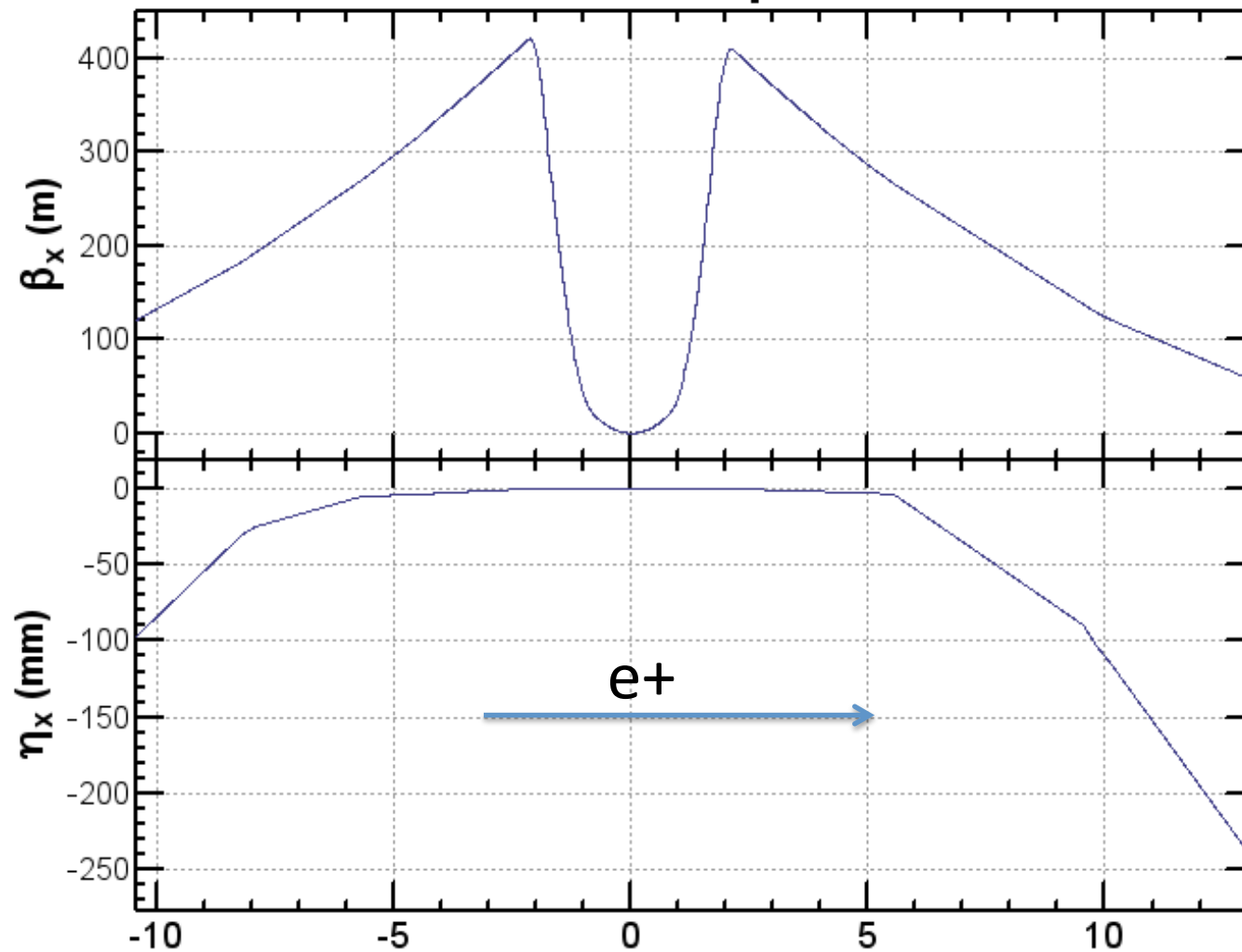


0.1mA/s -> 6.2GHz

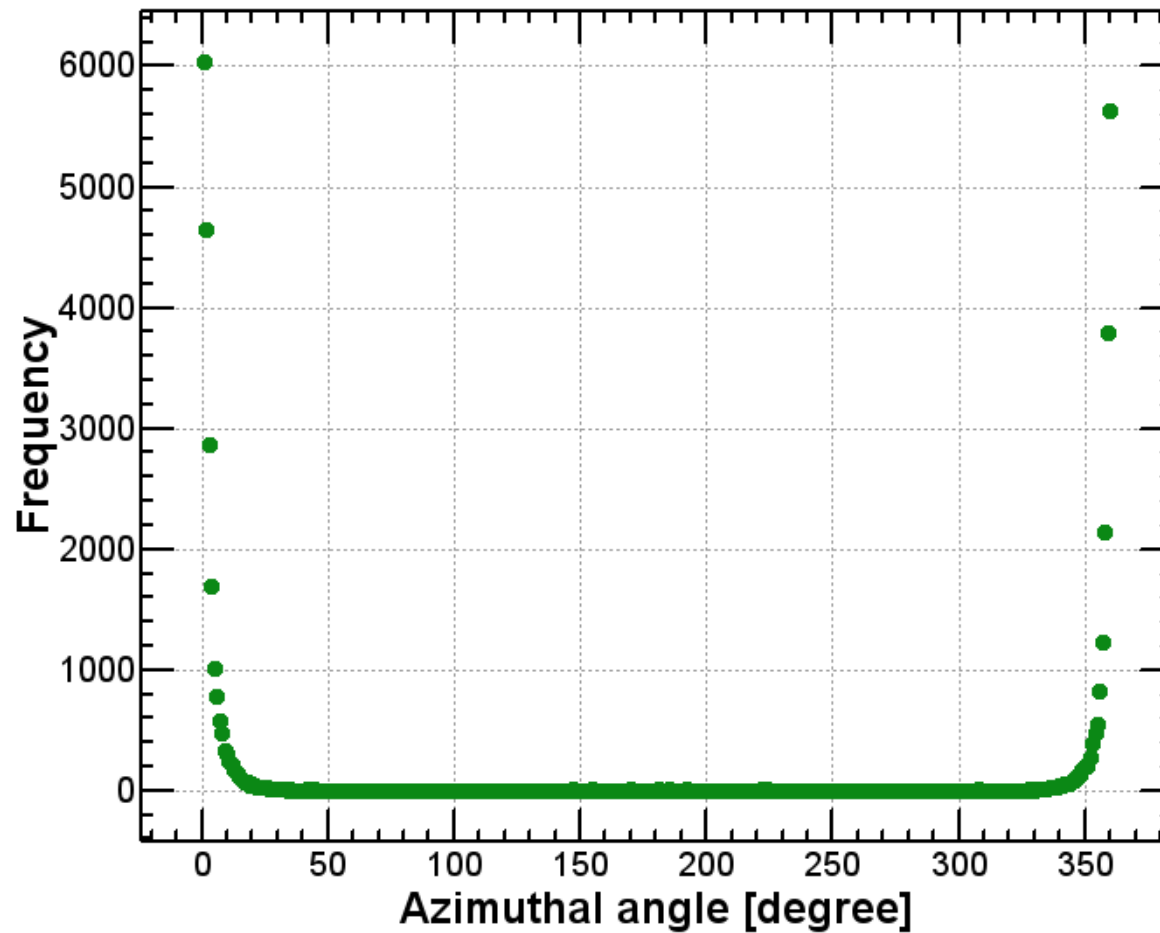
of survived particles (LER)



LER IR Optics



Azimuthal angle distribution of lost particles (LER)



Zero degree: horizontal (outside of ring)

Lost position: $4\text{m} < s < 16\text{m}$ from IP

Expected ZDLM rate (Uehara)

- Funakoshi-san's coefficient 0.1mA/s -> 6.2GHz
 - The rate should be proportional to luminosity
10³⁵ luminosity --- ~ 1GHz
 - Effective detector length --- ~ 0.1m
 - Efficiency --- 10%
(angular coverage and shower loss)
- Expected Rate --- 0.1mA/s → 10 MHz

LER 4 m point (upstream BLC1LP) ~ 2MHz @10³⁵
9 m point (downstream BLC1LP) ~ 2MHz @10³⁵

Luminosity Dithering Monte Carlo simulation

S.Uehara(KEK)

Parameters

- A set of measurement: measure the change of ZDLM rate for one second
- Sampling rate **1024Hz**
measure every 0.977ms
- Dithering — — frequency **$f = 77\text{Hz}$**
 $r \sim \sin 2\pi ft$

Assume that the luminosity depends on r with a Gaussian distribution.

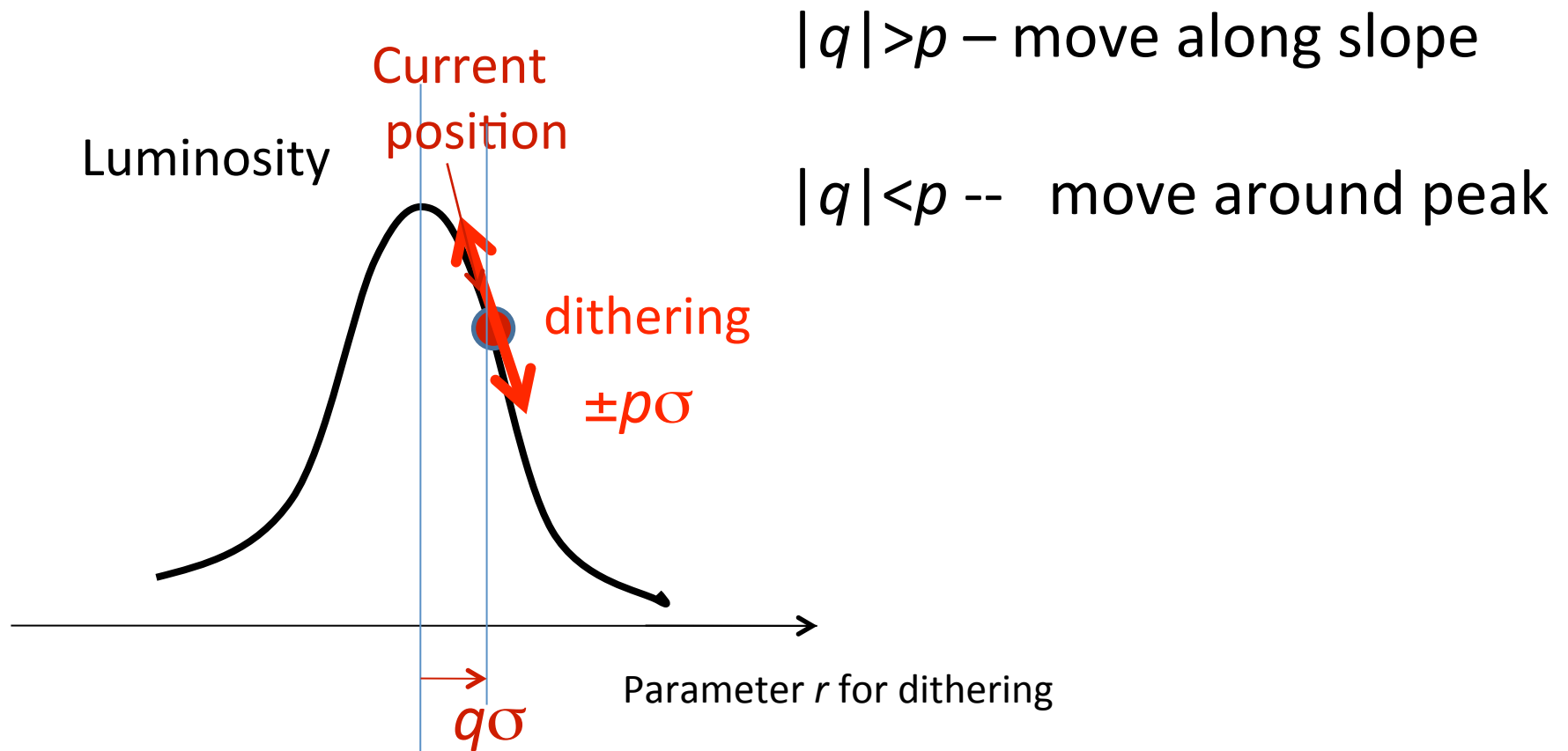
$$L(t) \sim \text{Exp}[-(q + p \sin 2\pi ft)^2/2]$$

q : offset

p : dithering amplitude

f : dithering frequency (here we assume $f=77\text{Hz}$)

Dithering



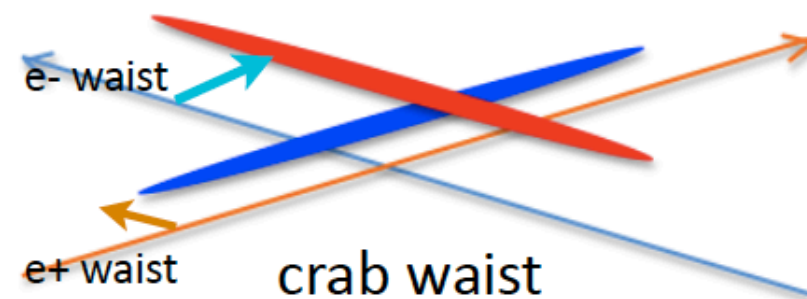
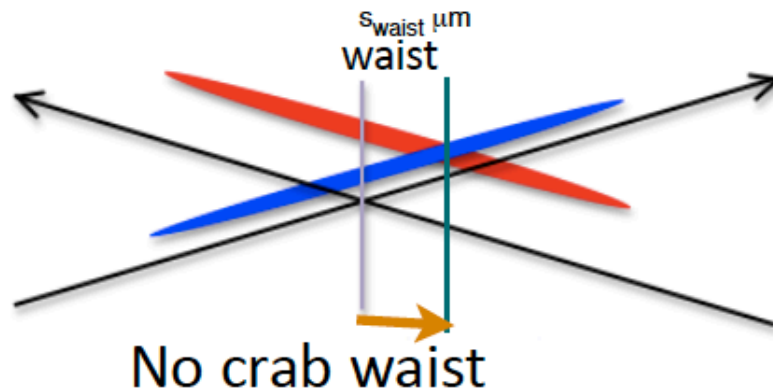
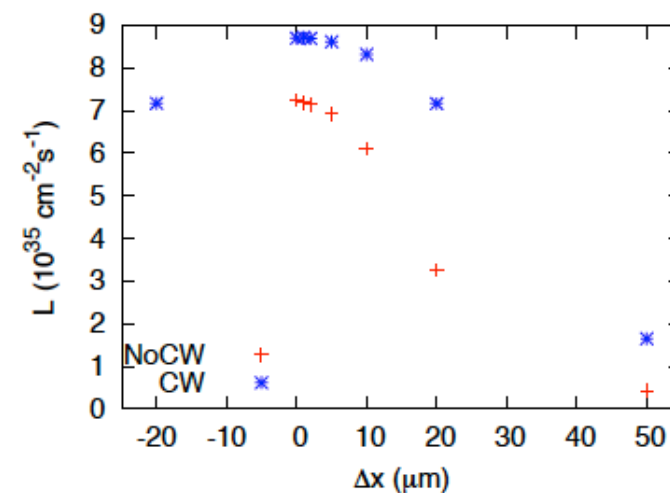
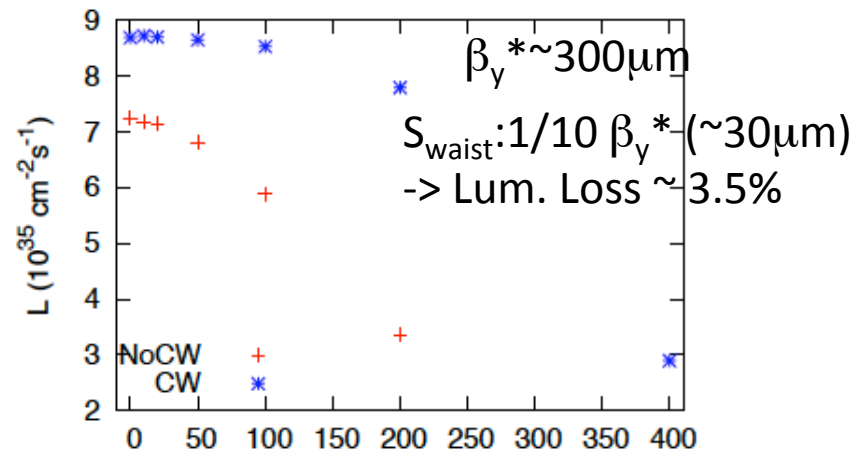
As for actual luminosity dependence on the orbit offset, we have to rely on the beam-beam simulation. Such simulation predicts that the luminosity loss with 1 σ_x offset is about 15%.

Tolerance of collision condition

K. Ohmi

Horizontal collision offset and waist

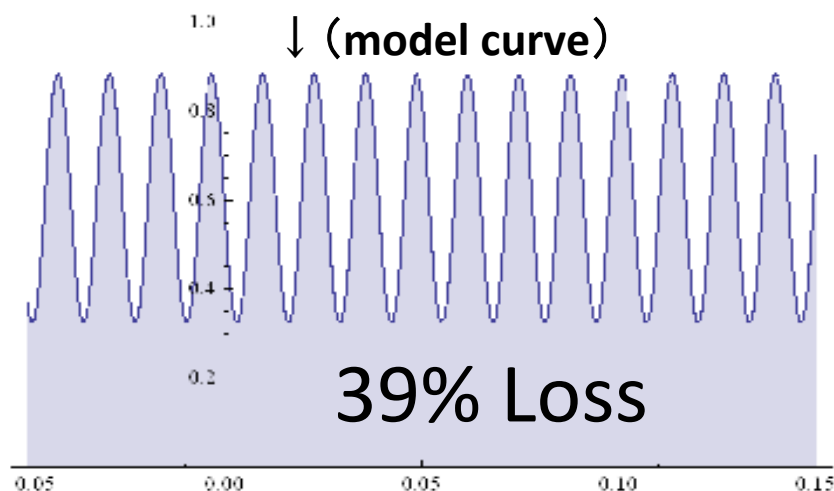
- Horizontal offset and waist are related to each other.
- The cross point of the waist is only one in x-z plane for the crab waist scheme.



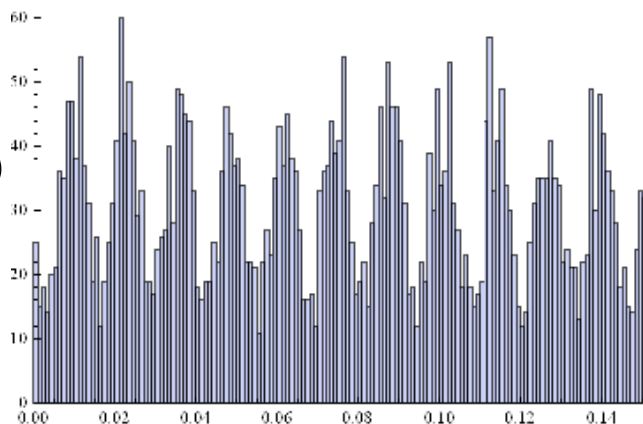
Result with Mathematica8

$p=0.5$, $q=1.0$, event rate=10kHz

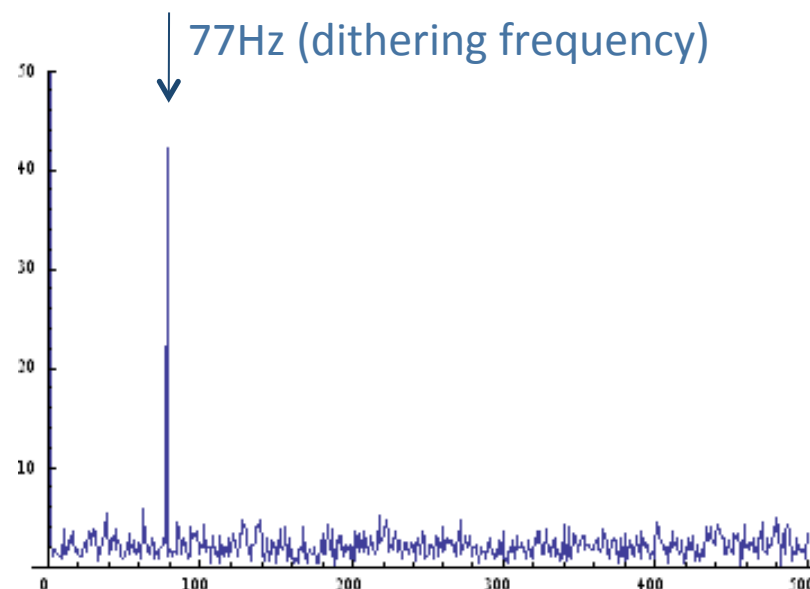
Luminosity



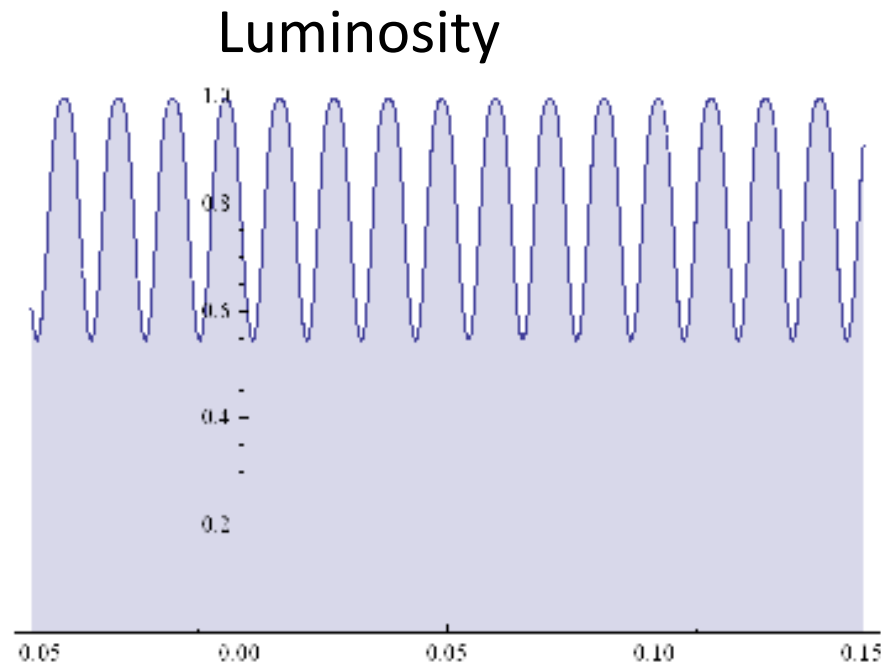
(MC data)



Sqrt of Power Spectrum

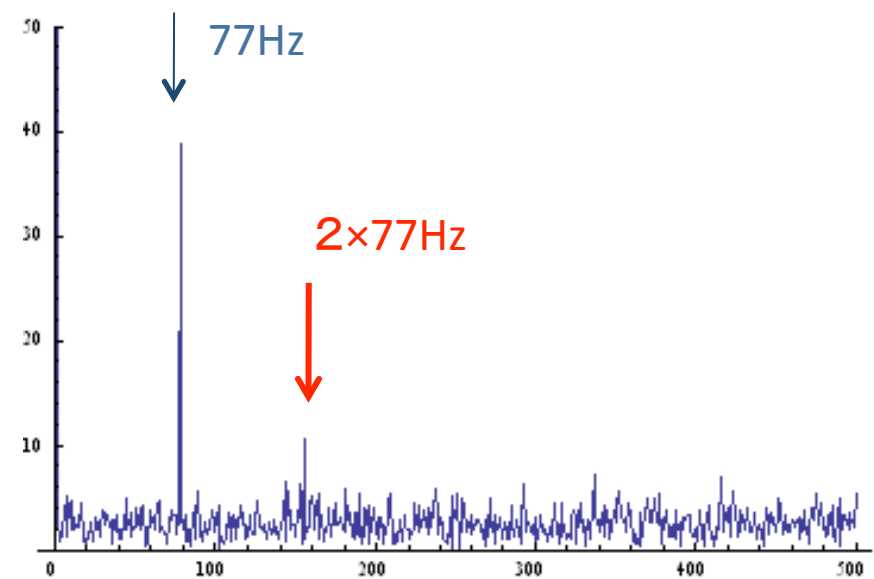


$p=0.5$, $q=0.6$, event rate=10kHz



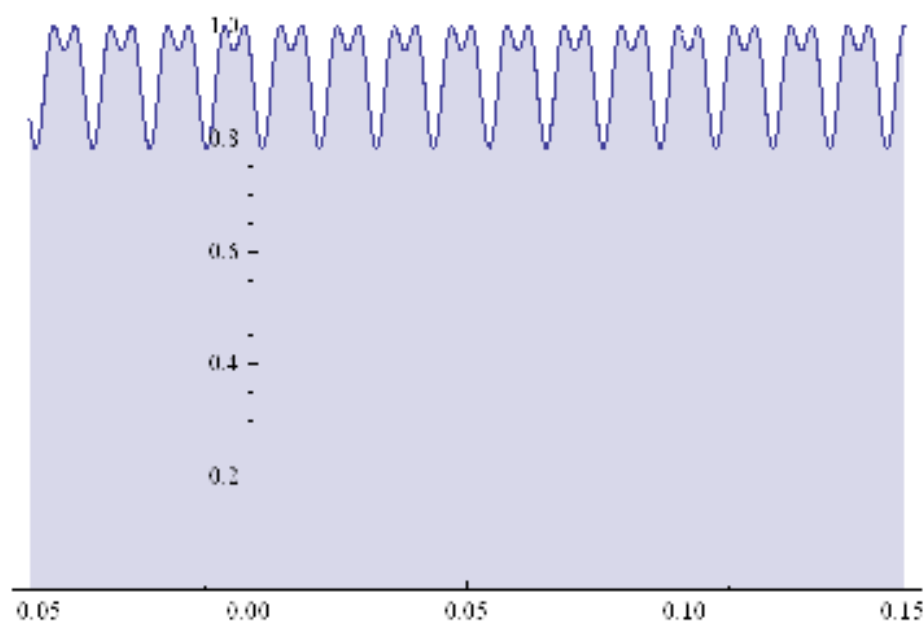
20% Loss

Sqrt of Power Spectrum



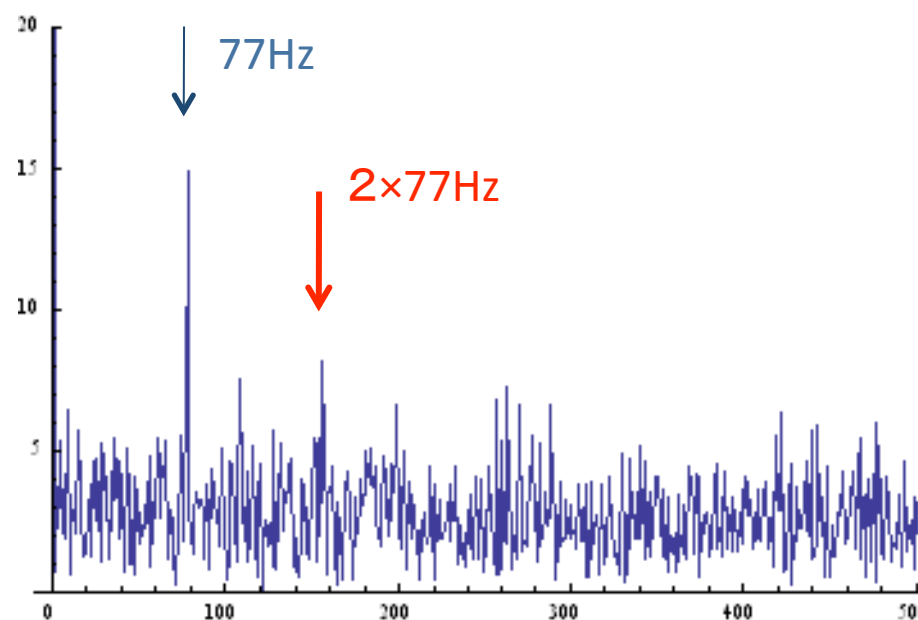
$p=0.5$, $q=0.2$, event rate=10kHz

Luminosity



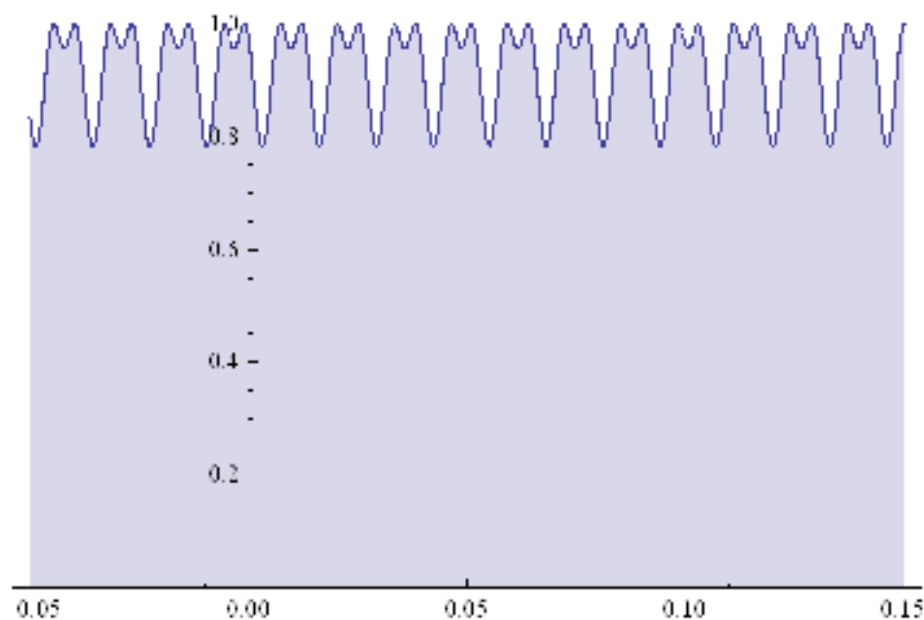
8% Loss

Sqrt of Power Spectrum



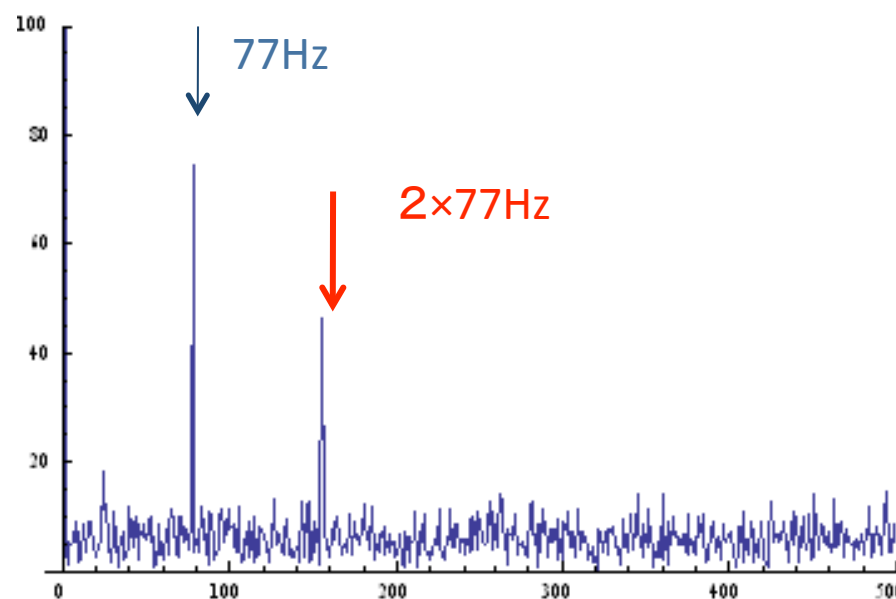
$p=0.5$, $q=0.2$, event rate=50kHz

Luminosity



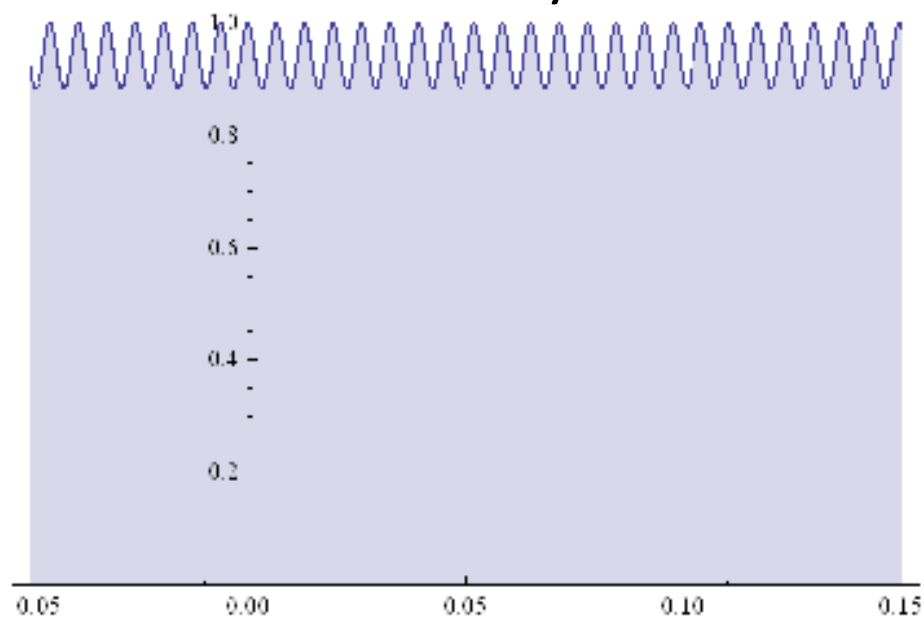
8% Loss

Sqrt of Power Spectrum



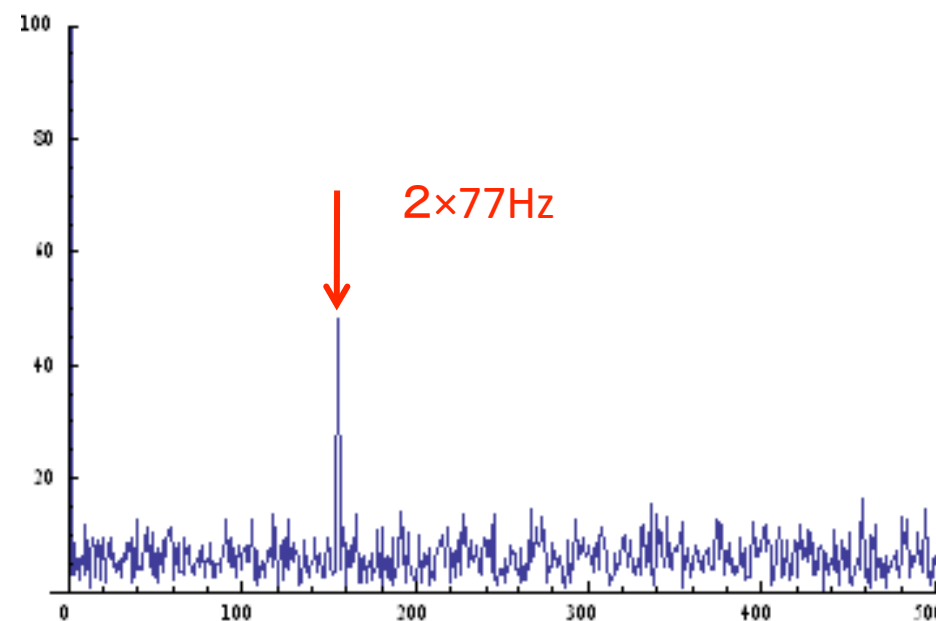
$p=0.5, q=0$, event rate=50kHz

Luminosity



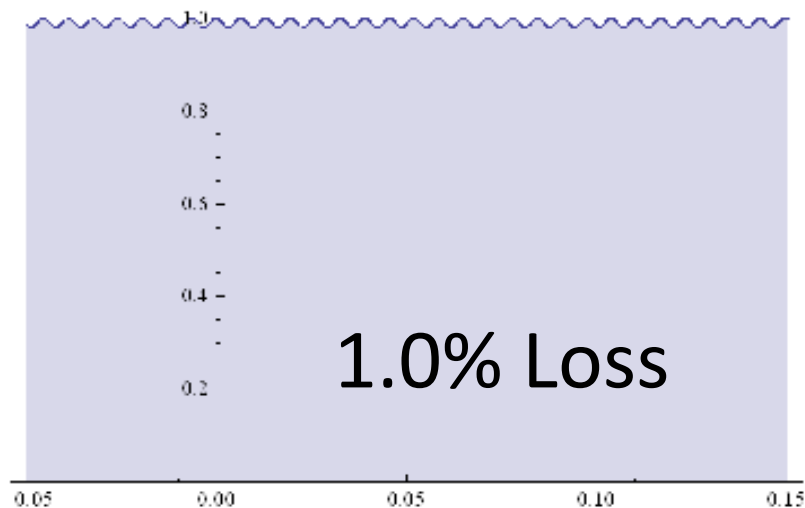
6% Loss

Sqrt of Power Spectrum

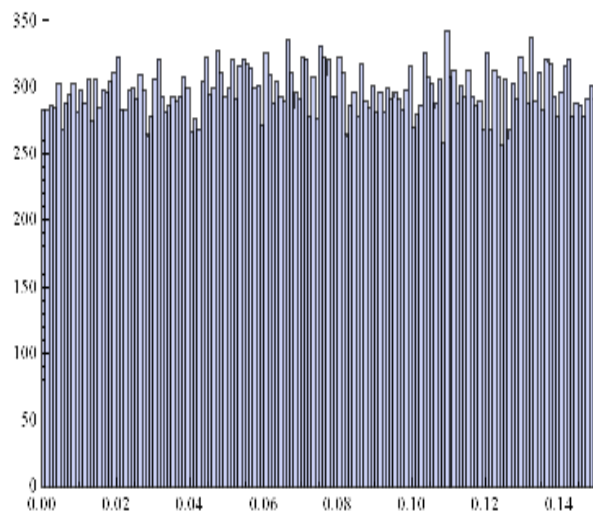


$$p = 0.2, q = 0$$

Luminosity



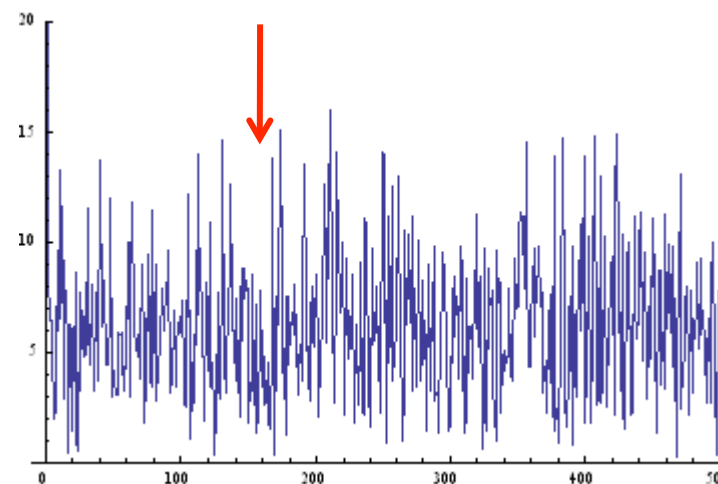
300kHz



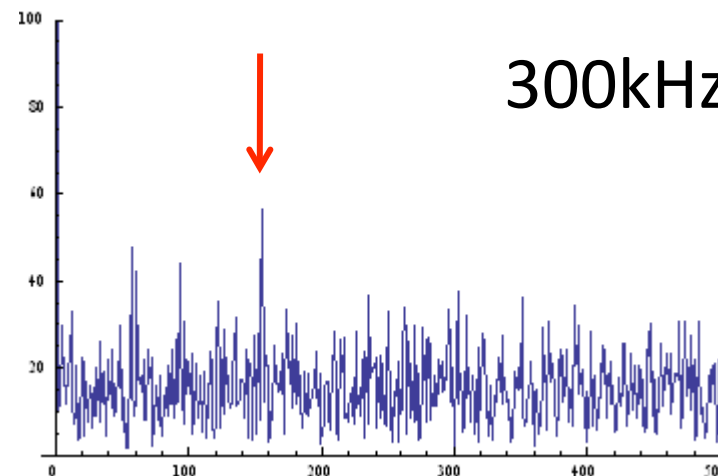
Sqrt of Power Spectrum

$2 \times 77\text{Hz}$

50kHz



300kHz



Conclusion of dithering simulation

- Dithering with 0.5σ amplitude
 - 50k event/s : OK
 - 10k event/s: not sufficient
 - Luminosity loss: $\sim 6\%$ at peak of luminosity
- Dithering with 0.2σ amplitude
 - We need $> 300\text{k event /s}$.
 - Luminosity loss: $\sim 1\%$ at peak of luminosity
- Expected event rate in case of measuring lost particles
 - $\sim 2\text{MHz @ } 10^{35} \text{ cm}^{-2} \text{ s}^{-1}$

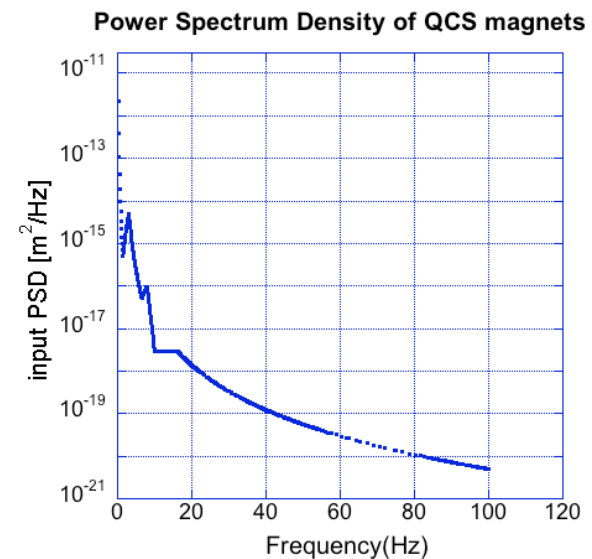
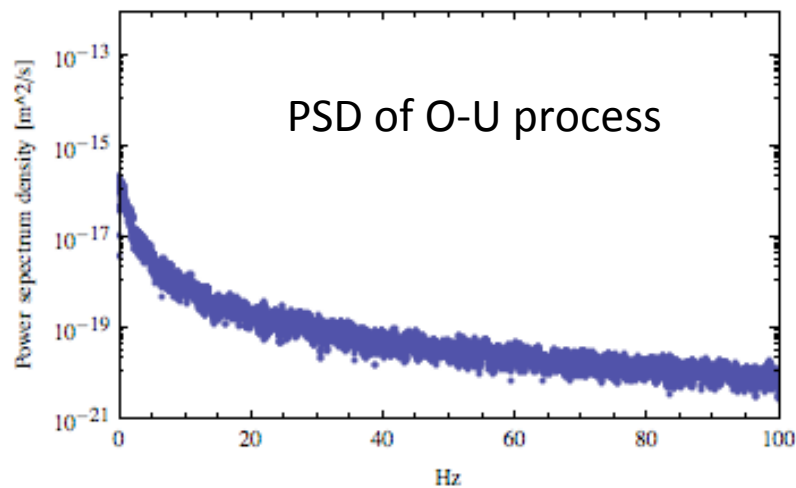
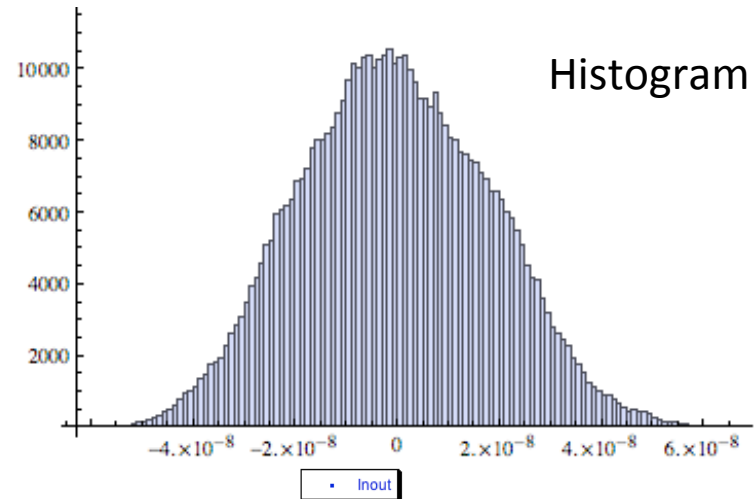
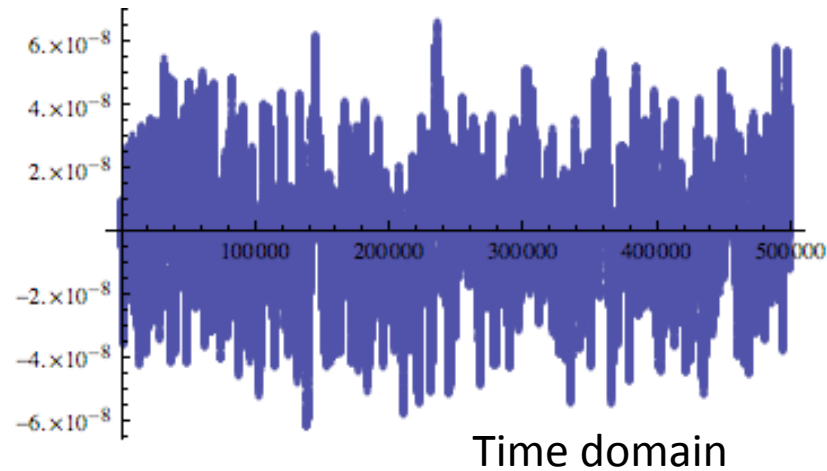
Summary

- Algorithm of orbit control
 - Vertical: beam-beam deflection based on BPM measurement
 - Horizontal: dithering method or beam size feedback
- QCS vibration issues
 - We found that coherency of QC1 and QC2 for electron and positron is almost complete on both sides of IP.
 - Further suppression of the vibration ($\sim 50\%$) is possible by using high damping material.
 - The coherence of vibration of the two rings may help.
- Dithering for horizontal orbit control
 - We just started considered the dithering method for horizontal orbit control.
 - Our study is on a primitive stage. We have conducted some simulations on the event rate of fast luminosity monitor.

Spare slides

Ground motion data created by using Ornstein-Uhlenbeck process

$\tau = 0.2$, $c = 1 \times 10^{-10}$, $\Delta t = 1/53/50$



Ornstein-Uhlenbeck process

- Measurement on ground motion
 - consistent with Brownian motion in low frequency region (S. Takeda)
- Brownian motion
 - Explained by Einstein using diffusion equation (1905)
 - Analyzed by P. Langevin using continuous Markov process (1908)
- Ornstein-Uhlenbeck process (sort of continuous Markov process)
 - Used in analysis of Brownian motion

$$X(t+dt) = X(t) - \tau^{-1}X(t)dt + c^{1/2}n(dt)^{1/2}$$

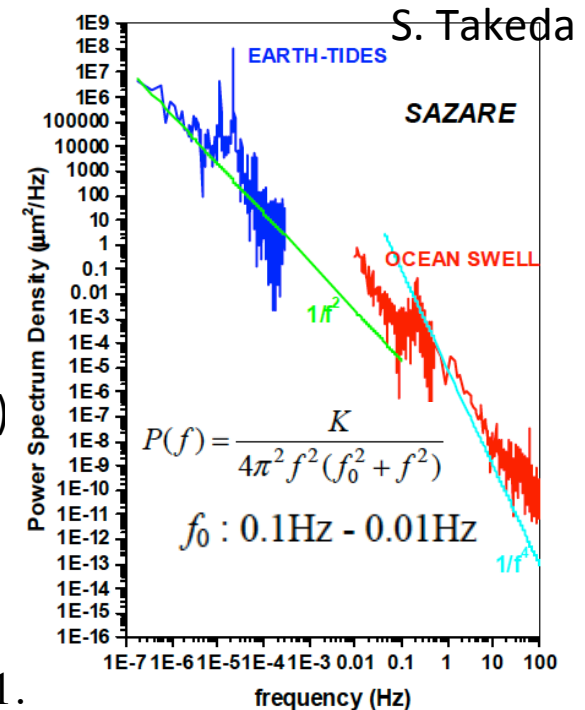
n : sample value of random variable $N=N(0,1)$

$N(0,1)$ is Gaussian distribution with mean=0, $\sigma=1$.

$$X(t+\Delta t) = X(t)e^{-(1/\tau)\Delta t} + \left[\frac{c\tau}{2} (1 - e^{-(2/\tau)\Delta t}) \right]^{1/2} n \quad (\leftarrow \text{Exact update formula})$$

$$\langle X(t) \rangle = x_0 e^{-(t-t_0)\tau} \rightarrow 0 (t \rightarrow \infty), \quad \text{var}\{X(t)\} = \frac{c\tau}{2} (1 - e^{-2(t-t_0)\tau}) \rightarrow \frac{c\tau}{2} (t \rightarrow \infty)$$

Power spectrum density $S_X(f) = \frac{2c\tau^2}{1 + (2\pi\tau f)^2} \sim \frac{1}{f^2}$



System of harmonic oscillator with damping and external force

- Modeling of magnet vibrations

$$y = \sum_{i=1}^n y_i \quad (i: \text{each resonant mode})$$

- Equation for y_i

$$\ddot{y}_i + \frac{2}{\tau_i} \dot{y}_i + \omega_i^2 y_i = C_i F$$

τ_i : damping time (determine Q value of resonance)

ω_i : angular resonant frequency

C_i : coupling between floor vibration and magnet

F : external force (substitute floor vibration data for this force)

- Solution of equation

- $\omega_i = 2\pi \times (3\text{Hz}, 36\text{Hz}, 53\text{Hz})$: solve with Runge-Kutta method
- Coupling and damping time were chosen so that the resonances are reproduced.
- Sum up three solutions

Summary of MAC in 2011

- The IP orbit control at SuperKEKB is much more difficult than that at KEKB.
- Major difficulty comes from the mechanical vibration of IR quadrupoles.
 - Simulation on the quads of SuperKEKB has given a better result than KEKB.
 - Further suppression of the vibration may be possible.
 - The coherence of vibration of the two rings may help.
- In parallel to the efforts to suppress the quadrupole vibration, we will develop the orbit feedback based on the beam-beam deflection.
- BPM requirement
 - Resolution: $1\mu\text{m}$ is enough. $5\mu\text{m}$ is tolerable?
 - Bandwidth: $\sim 1\text{kHz}$
- Horizontal orbit feedback
 - We need to develop a method other than the beam-beam deflection such as luminosity feedback or beam size feedback.

IP machine parameters

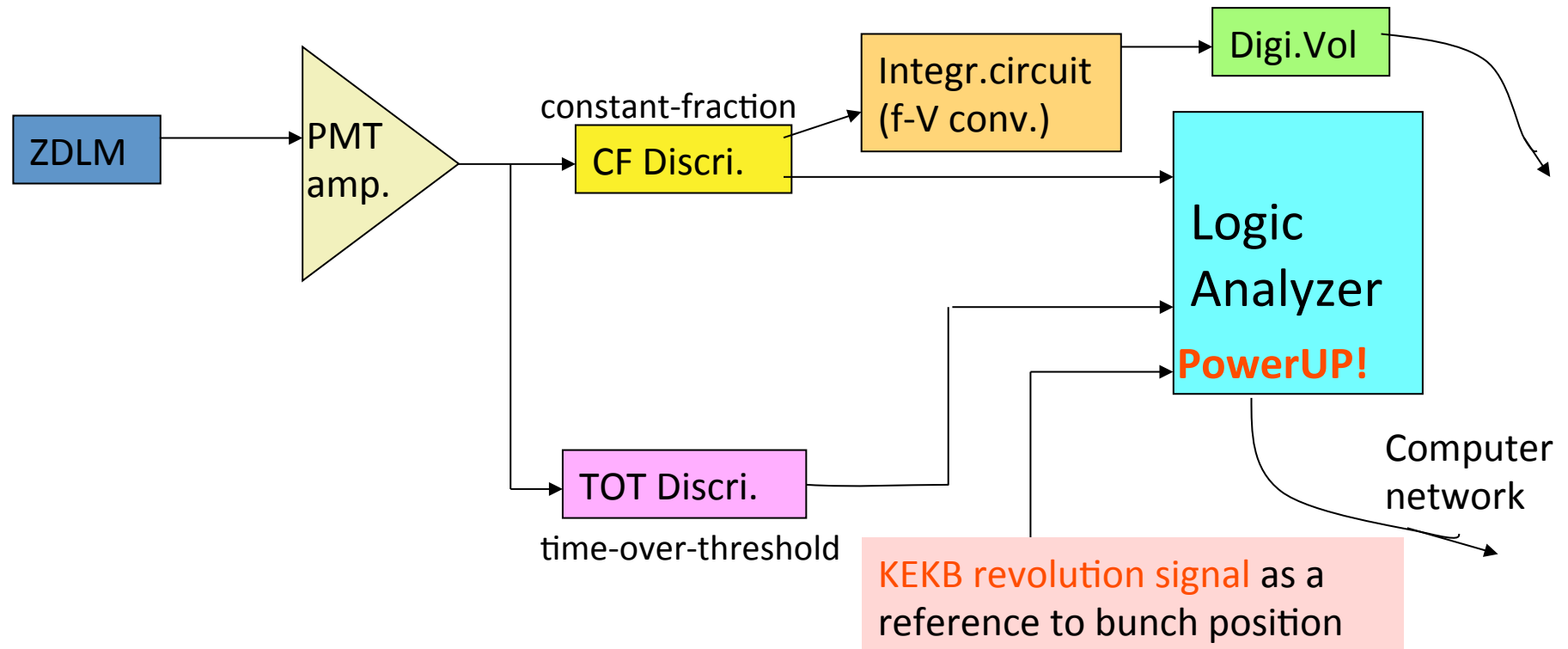
	KEKB		SuperKEKB	
	LER	HER	LER	HER
ϵ_x	18nm	24nm	3.2	5.0
ϵ_y	0.15nm	0.15nm	8.6pm	13.5pm ~1/4
κ	0.83 %	0.62%	0.27%	0.25%
β_x^*	120cm	120cm	32mm	25mm
β_y^*	5.9mm	5.9mm	0.27mm	0.31mm ~1/4.5
σ_x^*	150 μ m	150 μ m	10 μ m	11 μ m
$\sigma_x'^*$	120 μ rad	120 μ rad	450 μ rad	320 μ rad
σ_y^*	0.94 μ m	0.94 μ m	48nm	56nm ~1/20
$\sigma_y'^*$	0.16mrad	0.16mrad	0.18mrad	0.22mrad
iBump horizontal offset		+/- 500 μ m		+/- 30 μ m?
iBump vertical offset		+/- 150 μ m		+/- 7.5 μ m?
iBump vertical angle		+/- 0.4mrad		+/- 0.4mrad?

Measurements by ZDLM

Luminosity measurements

(1) Counting rate variation with continuous measurement

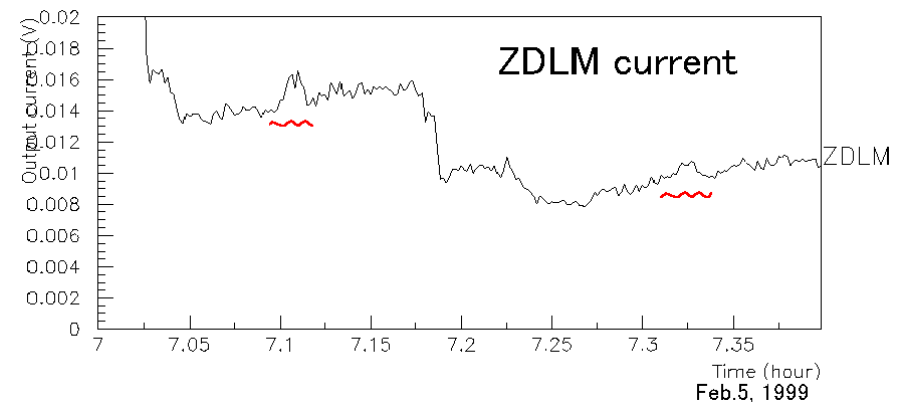
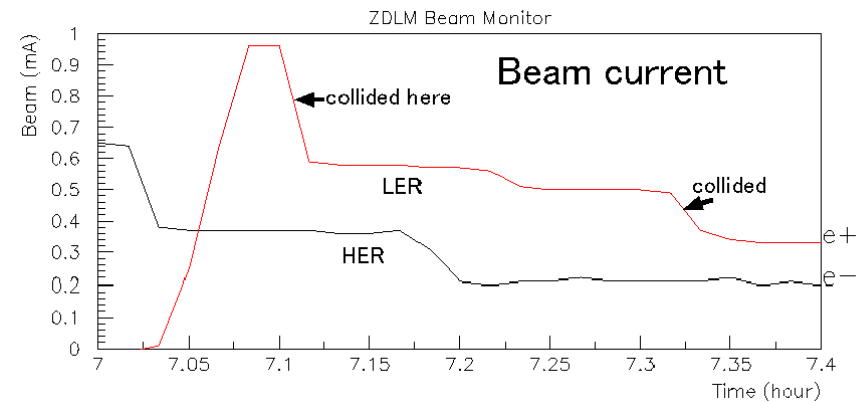
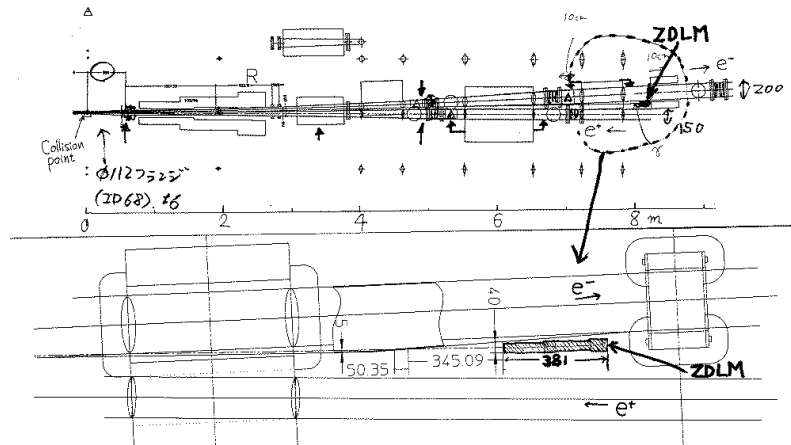
(2) Bunch-by-bunch Luminosity – time critical measurement
in rather short terms



ZDLM-1 in KEKB Commissioning

“Real-time luminosity monitor for a B-factory experiment”

T.Hirai, S.Uehara and Y.Watanabe, Nucl. Instr. Meth. A458 (2001) 670–676.



The first collision signal of KEKB
Before installation of Belle

ZDLM-5@KEKB/Belle in 2010

- Quartz Cherenkov radiator

on the deflected e- region (low efficiency)

(The photons were blocked by thick beam chamber (~ 15 r.l. Cu))

Can obtain the timing information

→ bunch-by-bunch luminosity measurement.

$\sigma_t = 0.5$ ns using a CF discriminator

Contributions from other magnets

- IP vertical orbit change due to $0.1\mu\text{m}$ position change
 - QC1LP ($\beta_y \sim 2519\text{m}$, $K_1 \sim 1.68$) $\rightarrow 69\text{nm}$ @ IP
 - QC5LP ($\beta_y \sim 1570\text{m}$, $K_1 \sim 0.15$) $\rightarrow 4.9\text{nm}$ @ IP
 - Q (typical in arc) ($\beta_y \sim 20\text{m}$, $K_1 \sim 0.2$) $\rightarrow 0.75\text{nm}$ @ IP
- Collective effects of many Q magnets
 - Number of Q magnets per ring: ~ 400
 - Assume no correlation of movements of the magnets:
 $\rightarrow$ expected offset at IP $\rightarrow 0.7 \times \text{Sqrt}(400) \sim 15\text{ nm}$

Effect of BPM resolution

