Optics Issues

2015.02.23 11:35 - 12:15 Akio Morita

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Belle II Solenoid Deformation (1)

- Belle detector solenoid coil geometry is designed symmetric, but ...
 - The center of measured Belle solenoid field is shifted about 440mm toward R-side(Oho side).
 - This field center shift corresponds with 30mm coil shift in 2D magnetic field calculation model.
 - This issue is figured out by Tsuchiya-san @ IR Tech. Meeting #96(2013.10.24)
 - We have to ...
 - Re-optimize current density distribution of compensation solenoid coils for adjusting Bz & JBz distribution
 - QCS(QC1 & QC2) geometry is already finalized.

Belle II Solenoid Deformation (2)

 The effect of the detector solenoid coil shift in 2D solenoid model



Belle II Solenoid Defomation (3)

• 3D solenoid field distribution on HER beam line before & after Belle II detector solenoid coil shift



Compensation Solenoid Coil Modeling Updates (1)

- The compensation solenoid coil modeling for 3D magnetic field calculation is updated by using coil geometry of hardware design.
 - It changes field distribution around QC1.
 - It changes IR orbit, coupling & dispersion functions.
 - We have to ...
 - Re-optimize current density distribution of compensation solenoid coil for adjusting Bz & JBz distribution
 - QC1/2 geometry is already finalized.
 - Re-match IR optics.
 - Re-optimize dynamic aperture & lifetime.

Compensation Solenoid Coil Modeling Updates (2)



from SuperKEKB IR Tech. Meeting #110(2014.7.17)

Compensation Solenoid Coil Modeling Updates (3)

Field distribution before/after L-side compensation solenoid coil modeling update.



Modeling Parameter Updates for Normal Conducting Magnets (1)

- Magnet group gives us the magnetic field measurement results of new magnets(dipoles and quadrupoles).
 - We have to update lattice modeling parameters for new magnets(We used temporary values for such magnets).
 - Effective length(L) and fringe length(F1) paramters change orbit geometry around dipole magnet, ring circumference and optical functions.

Modeling Parameter Updates for Normal Conducting Magnets (2)

- Status of model lattice updates
 - LER model update is completed.
 - HER model update is not complated yet.

Туре	Old L _{eff} (m)	New L _{eff} (m)	∆x _{center} (μm)◄	at the center of the magnet
B2P	4.189544	4.159654	210	
BLC1LP1	1.59	1.603162	40.8	Δx is acceptable.
BLC1LP2	2.23029	2.235386	6.18	It is negligible small compared with
BLCWRP	2.23029	2.235386	9.50	good field region.
BLC1RP	2.23029	2.235386	17.7	Realigement is not required!
BLA1LP	3.989597	3.961671	118	
BLX4RP	3.989597	3.961671	160	But, we MUST pay attention to
BLA6RP	3.989597	3.961671	176	magnet alignment with model
BC1LP	0.3444	0.281105	5.50	geometry.
BC1RP	0.3444	0.281105	2.84	Calculated by H.Sugimoto

Modeling Parameter Updates for Normal Conducting Magnets (3)

- LER circumference is extended about 800µm by dipole modeling parameter updates.
 - This displacement is not negligible compared with ±3mm tuning range of the LER chicane for adjusting circumference.
 - Total circumference difference between LER and HER is not confirmed because HER model updates is not completed yet.
 - We have extra circumference adjustment option by using wiggler K₀.



Touschek Lifetime with QCS Non-linear components (1)

- QC1LP & QC2LP multipole measurement results are released from SC group.
 - We have to check that the measured error is acceptable or not.
 - Both dynamic aperture & Touschek lifetime with multipole errors are evaluated by inserting thin multipole element to describe error field into every QCSs.

Touschek Lifetime with QCS Non-linear components (2)

QCS field measurement results by using harmonic coil

QC1LP with harmonic coll radius 12mm				QC2LP with harmonic coil radius 20mm						
	@ R = 10 mm , 4.2K and 1.8 kA		Design @ R= 10 mm				@ R = 30 mm , 4.2K and 1 kA		Design @ R= 30 mm	
	a _n skew	b _n	a _n	b _n			a _n	b _n	a _n	b _n
n=1	0.0	0.0	0.0	0.0		n=1	0.0	0.0	0.0	0.0
2	0.0	<u>10000</u>	0.0	<u>10000</u>	reference	2	0.0	10000	0.0	10000
3	0.40	3.16	0.0	0.0		3	1.79	-0.59	0.0	0.0
4	1.57	0.75	0.0	0.24		4	0.00	0.45	0.0	-0.06
5	-0.07	-0.42	0.0	0.0		5	-0.39	-0.17	0.0	0.0
6	-0.41	0.06	0.0	0.54		6	-0.14	3.54	0.0	0.28
7	0.05	0.05	0.0	0.0		7	0.32	-0.10	0.0	0.0
8	0.19	0.07	0.0	0.01		8	0.14	-0.23	0.0	0.11
9	-0.07	-0.04	0.0	0.0		9	0.22	0.03	0.0	0.0
10	0.00	0.03	0.0	-0.21		10	0.15	-1.41	0.0	-1.43

Large errors are found in sextupole & octupole mode(n=3,4).

- We CAN re-optimize dynamic aperture by using normal & skew sextupole coil and normal octupole coil in QCS and sextupole families in arc section. *from SuperKEKB IR Tech. Meeting #107(2014.6.5)* Touschek Lifetime with QCS Non-linear components (3)

- Touschek lifetime is evaluated by using model lattice with 4 thin multipole element to describe multipole errors for QC2R, QC1R, QC1L and QC2L.
 - The error field strength is fixed.
 - The worst set of the error field sign is selected from possible combinations.(evaluate worst case)



from SuperKEKB Optics Meeting #106(2014.9.17)

Touschek Lifetime with QCS Non-linear components (4)



Touschek Lifetime with QCS Non-linear components (5)



Sher 5769.sad

Dynamic Aperture with Crab Waist (1)

- The crab waist optics designs for Higgs factory collider were reported with enough dynamic aperture.
 - In those design, a set of sextupoles is used instead of single sextupole for compensating the thickness effect of the sextupole magnet.

Question

- Is those compensation scheme applicable to SuperKEKB?
- What is the difference between SuperKEKB and other collider?

Dynamic Aperture with Crab Waist (2)

- Those compensation scheme WOULD be inapplicable to SuperKEKB.
 - Compensation for crab waist sextupoles
 - The on-momentum aperture of SuperKEKB lattice with crab waist constructed by thin sextupoles is degraded.
 - Compensation for local chromaticity correcoters
 - The on-momentum aperture of SuperKEKB lattice with crab waist that does not contain LCC between crab waist sextupoles is degraded.
 - In the SuperKEKB design, $K_2\beta_y$ product at the LCC sextupole was reduced by increasing the horizontal dispersion function η_x in order to avoid the on-momentum aperture degradation by the sexutpole thickness effect.

Dynamic Aperture with Crab Waist (3)

Comparison of dynamic aperture limit by the fringe field of final focus quadrupole

 $J_y \leq \frac{\beta_y^{*2}}{(1+2|K|L^{*2}/3)L^*} A(\mu_y) \quad \text{ A}$

 $A(\mu)$: universal function

K. Oide et al, Phys. Rev. E47 (1993)

Ring	β_{y}^{*} [µm]	K=k ₁ [m ⁻²]	L* [m]	$J_y/A [\mu m]$		
SuperKEKB HER	300	-3.1	1.22	0.018		
SuperKEKB LER	270	-5.1	0.76	0.032	▲ 1/20	
CEPC	1200	-0.176	1.5	0.76		< 1/100
TLEP(BINP design)	1000	-0.16	0.7	1.36		< 1/100
KEKB	5900	-1.779	1.762	4.22		

- The final focus fringe of SuperKEKB is very strong compared with other e⁻ - e⁺ colliders.
- This strong fringe effect WOULD be the source of dynamic aperture difference under crab waist.

Emittance with Tunnel Subsidence



Tunnel subsidence model is generated from latest measurement with LPF($\lambda_{cut} \sim 100m$).

Vertical emittance after correction WOULD be improved into acceptable level by improving both local alignent around V-LCC and correction algorithm. (high β_v region)

Already reported in 18th Review

from TUPPC018 @ IPAC '12

Emittance with Machine Error (1)

Assumption of Machine Error(Random Error) Simulation

	Element Type	Δx _{rms} [µm]		Δy _{rr}	_{ns} [µm]	$\theta_{\rm rms}$ [mrad]	(∆K/K) _{rms}	
Machine Error	Main dipole	-			-	0.1	3.5 x 10 ⁻⁴	
	Quadrupole	100			100	0.1	7 x 10 -4	
	Sextupole	100			100	-	1.3 x 10 ⁻³	
	QC1 & QC2	100			100	-	-	
	BPM		75		75	1.0	-	
	Corrector Type	Э	HER	LER		Maximum Rating		
	H-Dipole		218	208		$\Delta \theta = 1.0 \text{ mrad}$		
	V-Dipole		196	215		$\Delta \theta = 1.0 \text{ mrad}$		
# of Correctors	H-Backleg Dipol	е	33	39		$\Delta \theta = 0.5 \text{ mrad}$		
	Quadrupole		292	254		$\Delta K_{1}/K_{1} = 5 \times 10^{-3}$		
	Skew Quadrupo	le*	64	56	ΔK ₁ =	$= 5 \times 10^{-3} \text{ m}^{-1} \text{ for SD,SL}$		
dy reported in 10th E	* We have addit but power suppl	iona y fo	al skew r skew	quadı quadr	upole coupole or	oil on SF type n SF is not re	e sextupole, ady at $T = 0$.	

Already reported in 19" Review

from SuperKEKB TDR draft

Emittance with Machine Error (2)

Vertical emittance and dynamic aperture after orbit & optics correction



 δ/σ_{δ} from SuperKEKB TDR draft

Summary of Past Emittance Study

- From orbit & optics correction study fortunnel subsidence
 - Vertical emittance WOULD be controled within acceptable level by taking extra care to V-LCC region.
- From orbit & optics correction study for random machine error
 - Vertical emittance reachs design target.
 - The sextupole tuning is required to obtain longer lifetime.

Tasks toward Machine Operation

- We have started to develop operation & commissioning softwares.
 - Optics & Orbit parameter management framework *under development*
 - Operation & Tuning Tools
 - Programable Tune Changer *under development*
 - Optics Measurement & Correction Toolset
 - Chromaticity Tuning Tool
 - Continuous Orbit Corrector
 - Local Orbit Bump Tool
 - Luminosity tuning Knobs(Waist, IP coupling, beam size...) *under development*
 - Calibration Tools(3-BPM, BBA...)
 - etc...

We plan to share framework software between MR and DR.